

Precise IV testing of BC solar cells: Challenges and status at ISFH

Karsten Bothe and David Hinken



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Accreditation



The Deutsche Akkreditierungsstelle GmbH attests that the calibration laboratory

Institut für Solarenergieforschung GmbH
ISFH Calibration and Test Center (CalTeC)
Am Ohrberg 1, 31860 Emmerthal

is competent under the terms of DIN EN ISO/IEC 17025:2018 to carry out calibrations in the following fields:

High Frequency – and radiation quantities

optical quantities

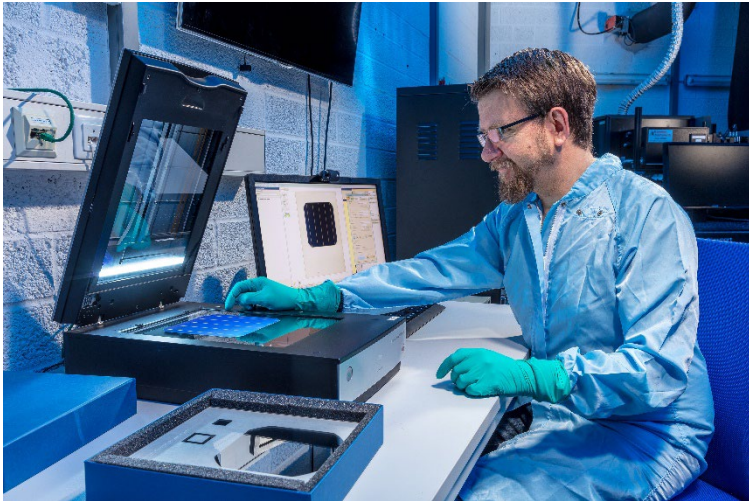
- photovoltaics
- radiometry

- ISFH CalTeC is ISO/IEC 17025 accredited
- The solar cell calibration laboratory is accredited by the German accreditation body DAkkS since 2016



Calibration of solar cells in three steps

Area (cell (TA) or mask (DA)) → Spectral Responsivity → Current-Voltage Characteristic



- Required for efficiency calculation



- Required for spectral mismatch correction
- Provides information about linearity



- Required for determination of characteristic parameters I_{sc} , V_{oc} , P_{max} , FF and efficiency

Calibration of solar cells in three steps

Area (cell (TA) or mask (DA))

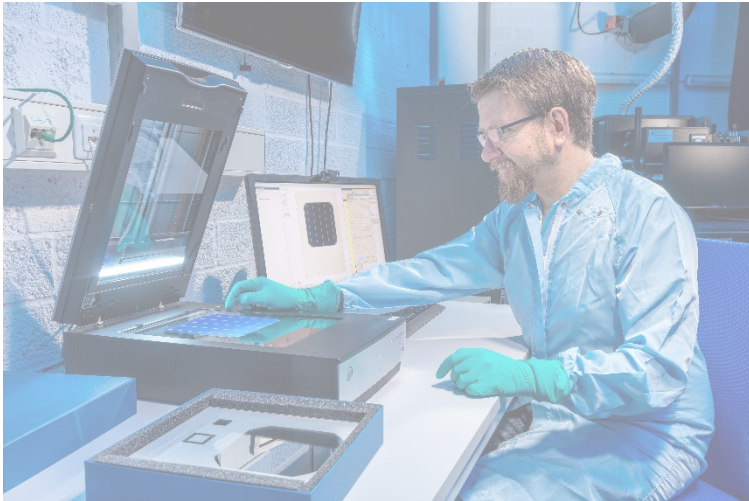


Spectral Responsivity



Current-Voltage Characteristic

1.



- Required for efficiency calculation



- Required for spectral mismatch correction
- Provides information about linearity



- Required for determination of characteristic parameters I_{sc} , V_{oc} , P_{max} , FF and efficiency

Calibration of solar cells in three steps

2.

Area (cell (TA) or mask (DA))

Spectral Responsivity

Current-Voltage Characteristic



- Required for efficiency calculation

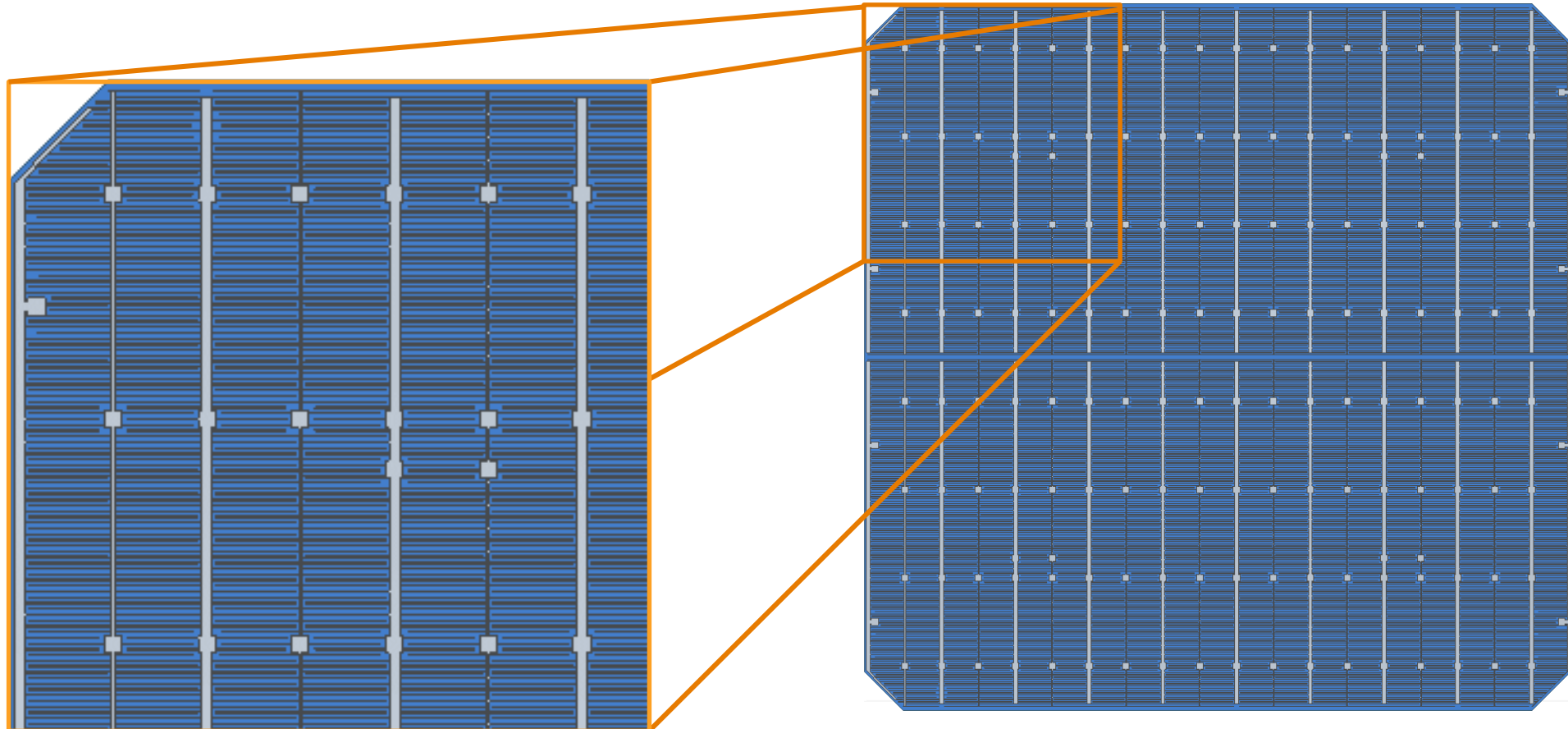


- Required for spectral mismatch correction
- Provides information about linearity



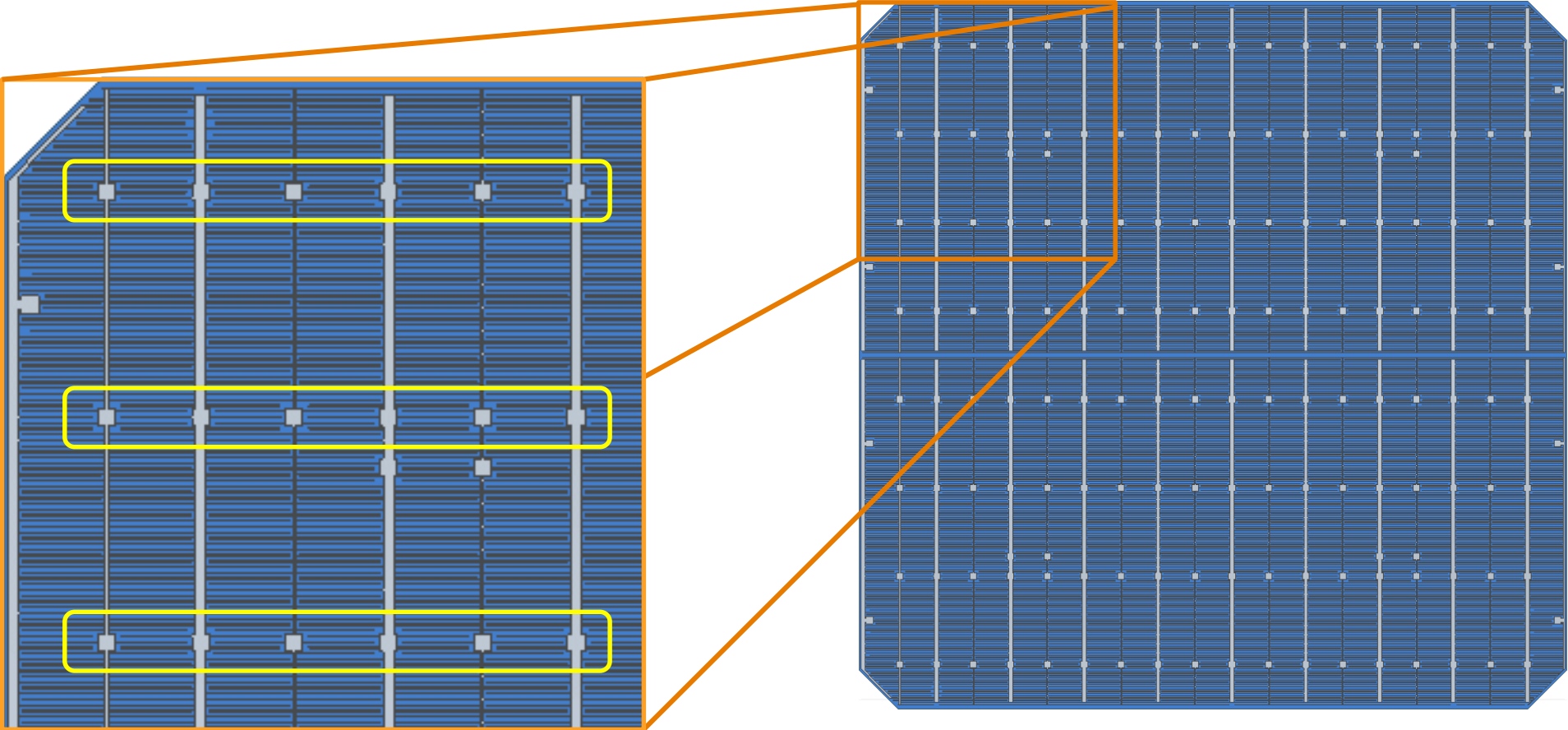
- Required for determination of characteristic parameters I_{sc} , V_{oc} , P_{max} , FF and efficiency

Metallisation layout

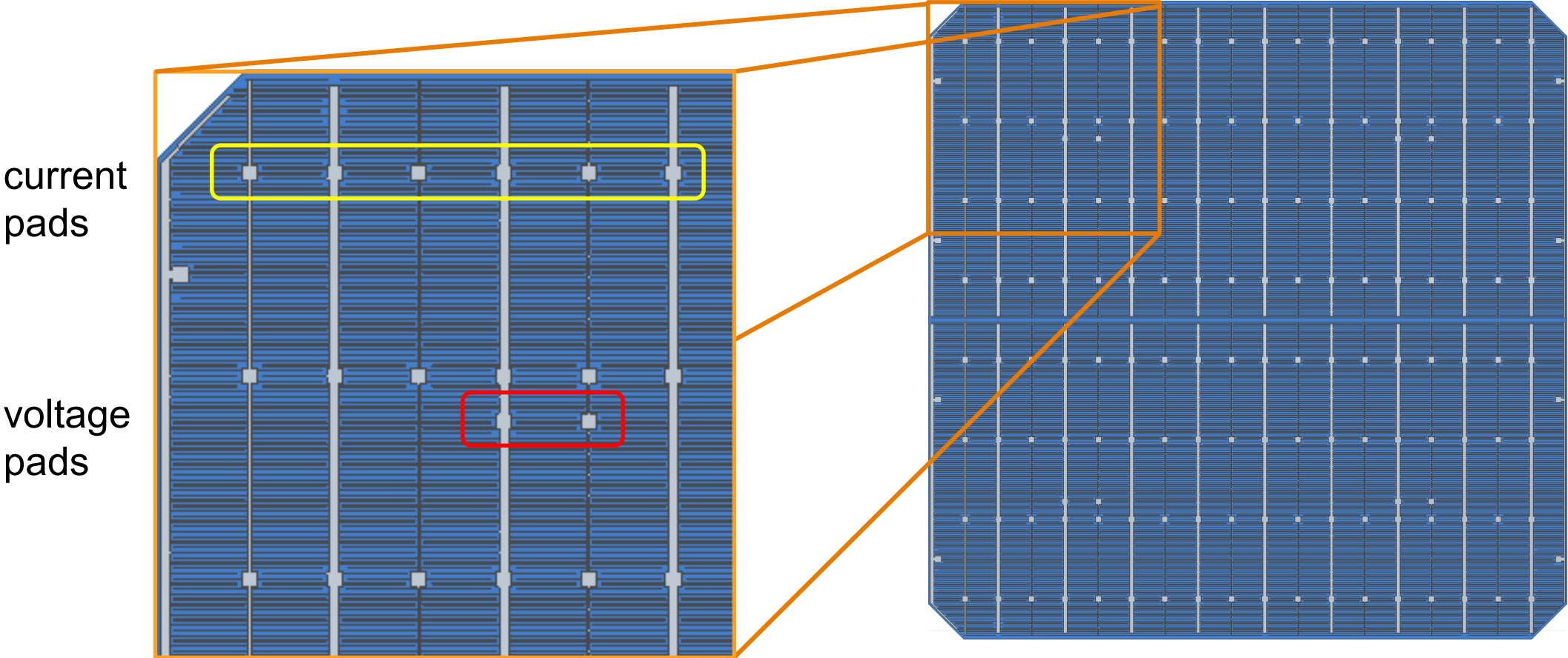


Metallisation layout

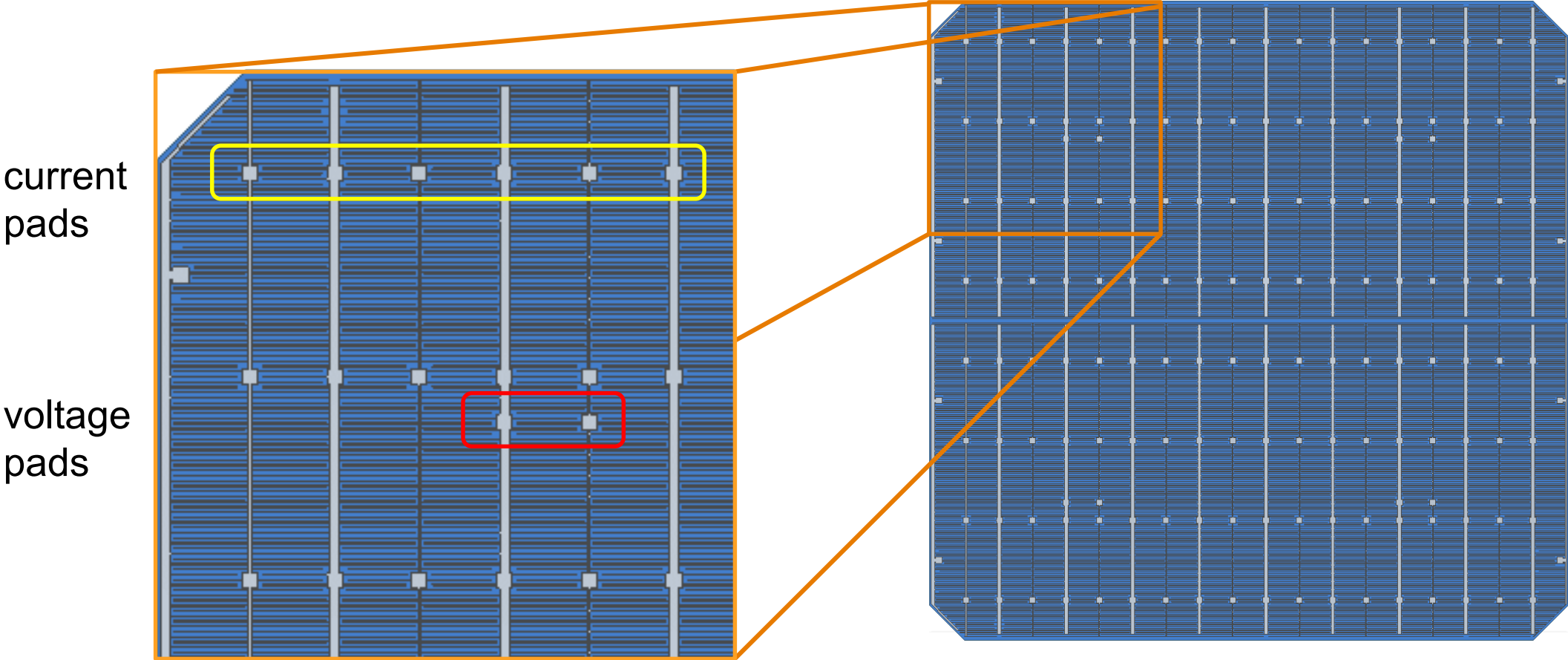
current pads



Metallisation layout



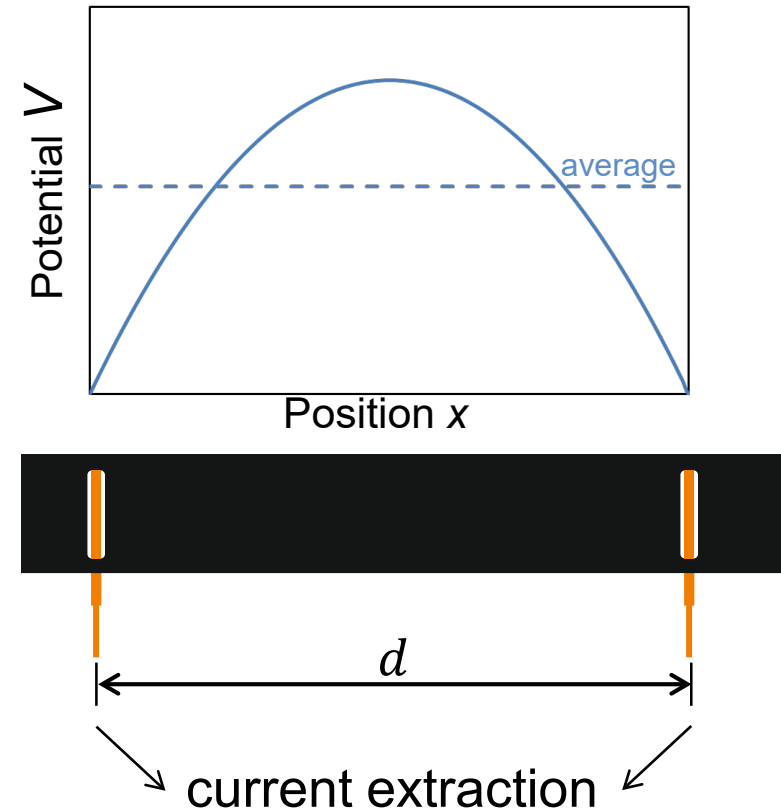
Metallisation layout



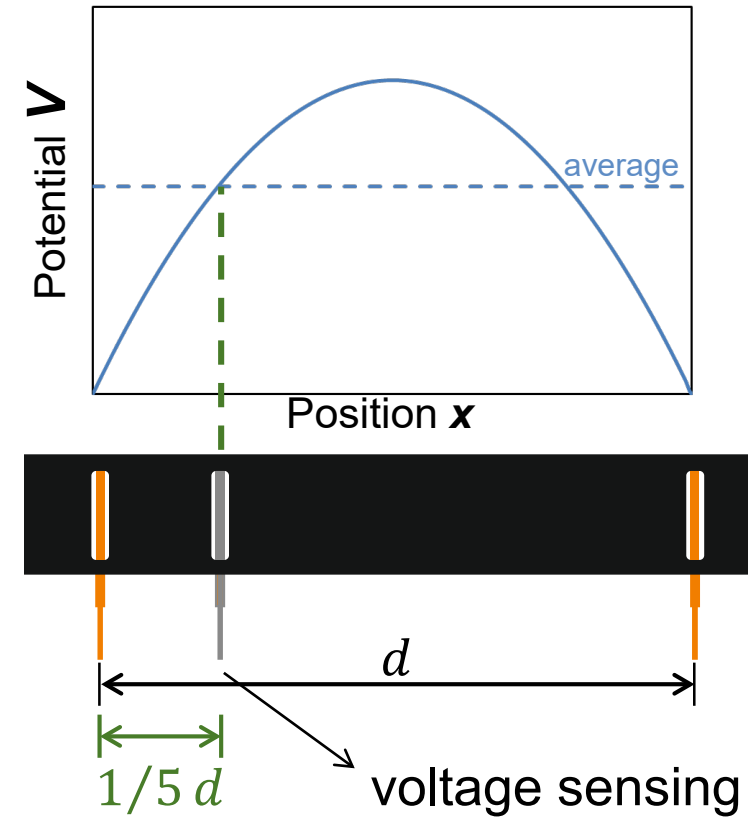
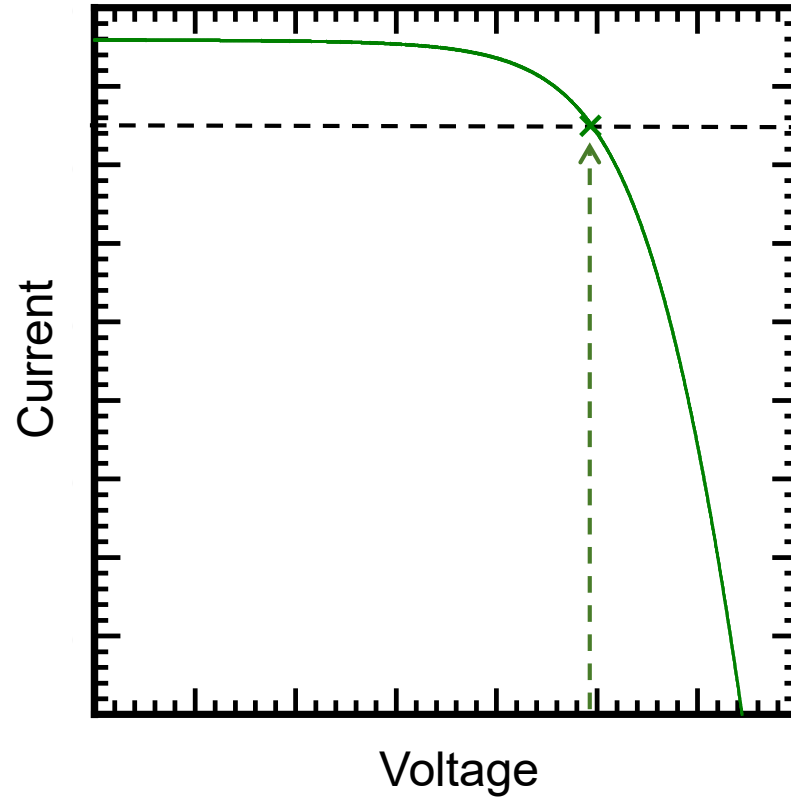
Where to place voltage pads for correct sensing?

FF over- and underestimation

- The sensing aims at probing the average busbar potential

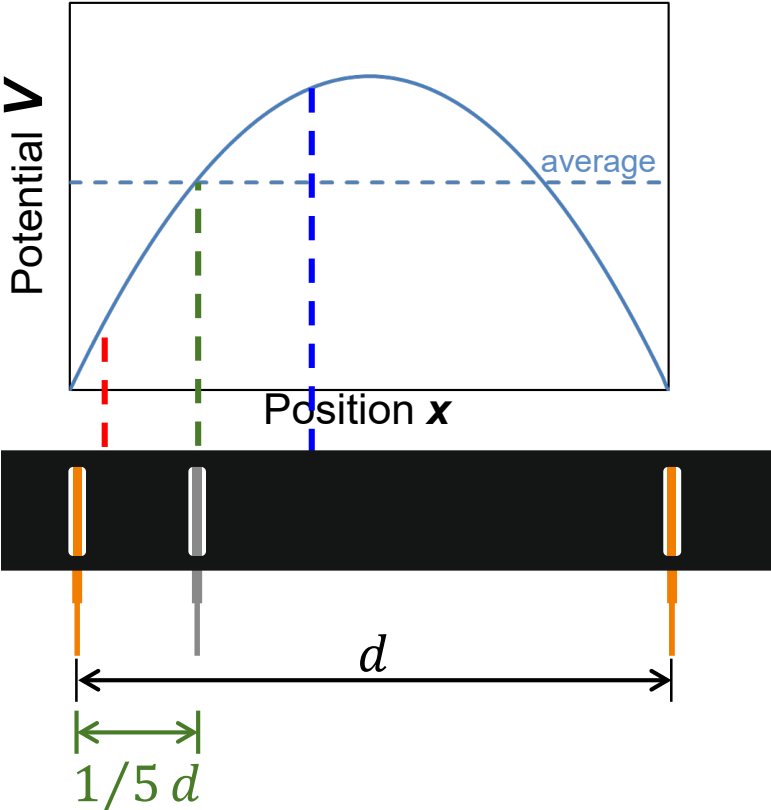
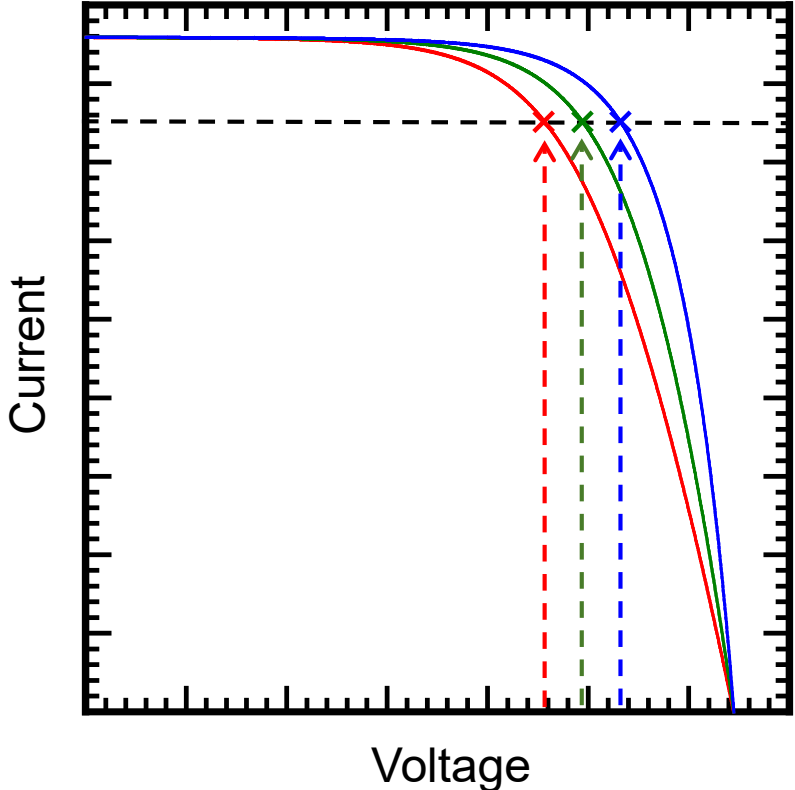


FF over- and underestimation



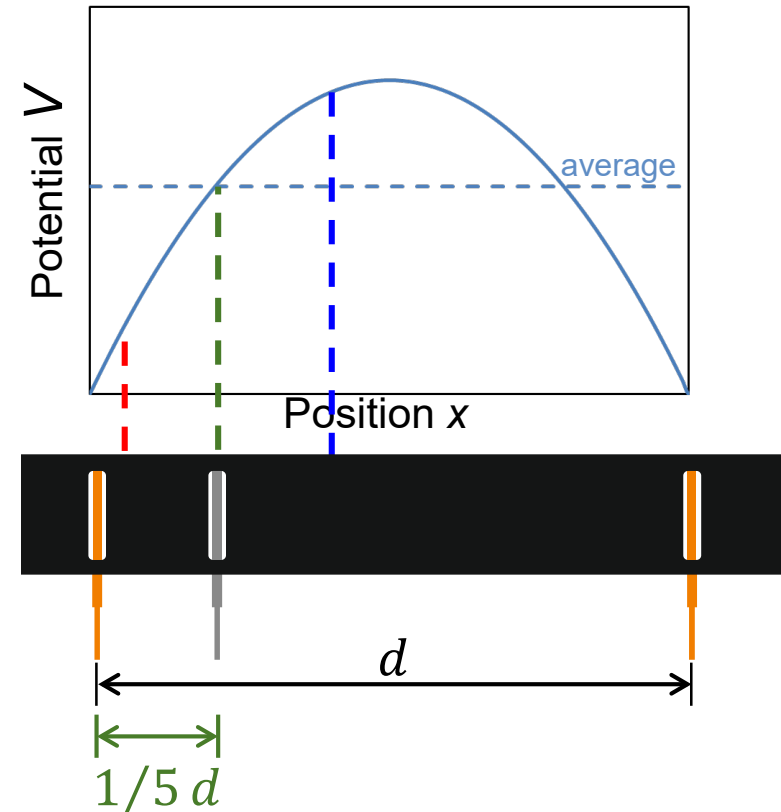
$$\frac{3-\sqrt{3}}{6} d \approx 0.211 d \approx 1/5 d$$

FF over- and underestimation

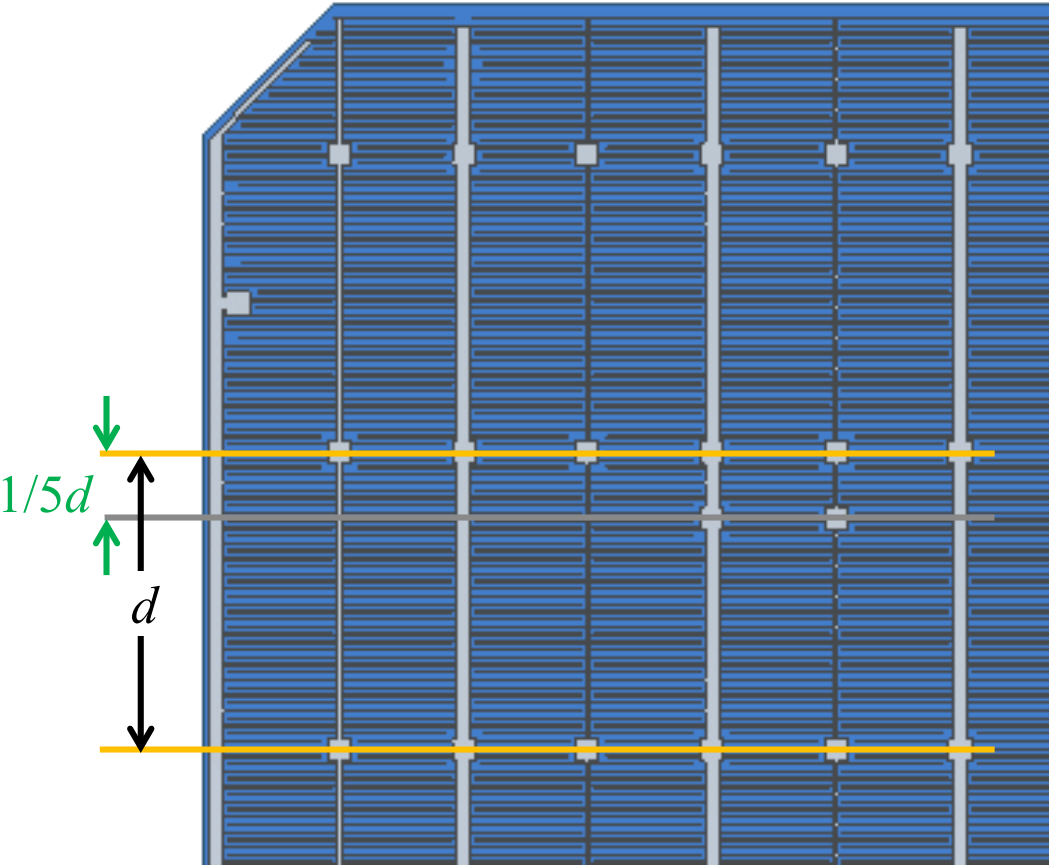


- The sensing aims at measuring the potential that would be measured if the entire busbar were contacted
 - Sensing on busbar with at $1/5^{\text{th}}$ of the distance of two adjacent contacting probes
 - The measured FF is independent of the actual busbar resistance and number of probes

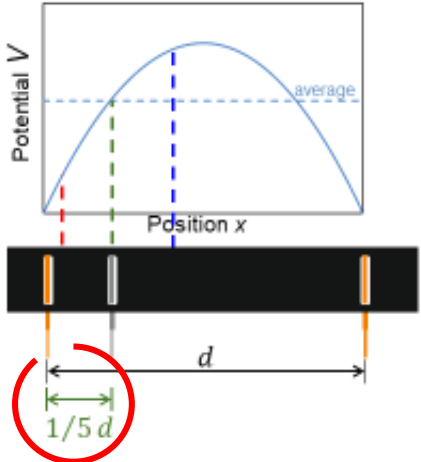
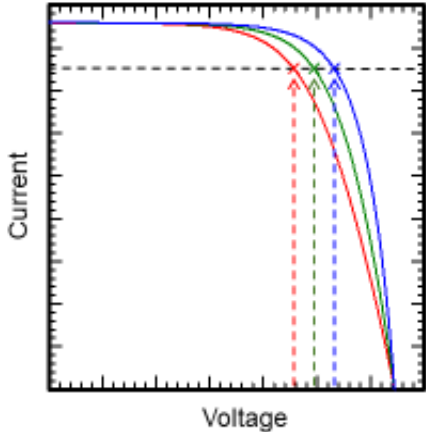
→ Busbar-resistance neglecting (brn) contacting



Back contact cells



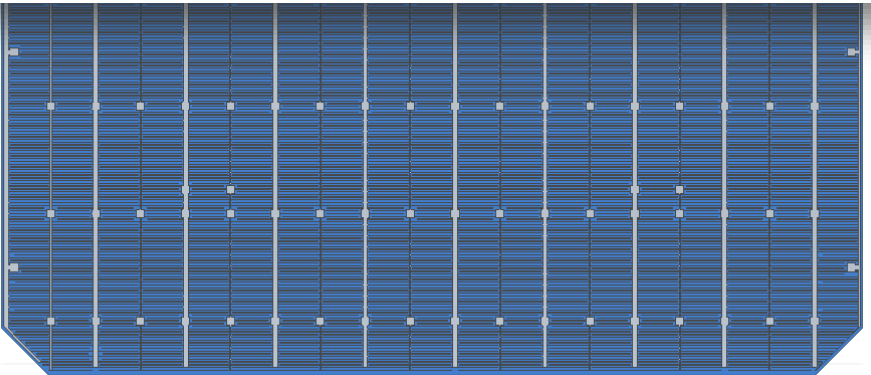
FF over- and underestimation



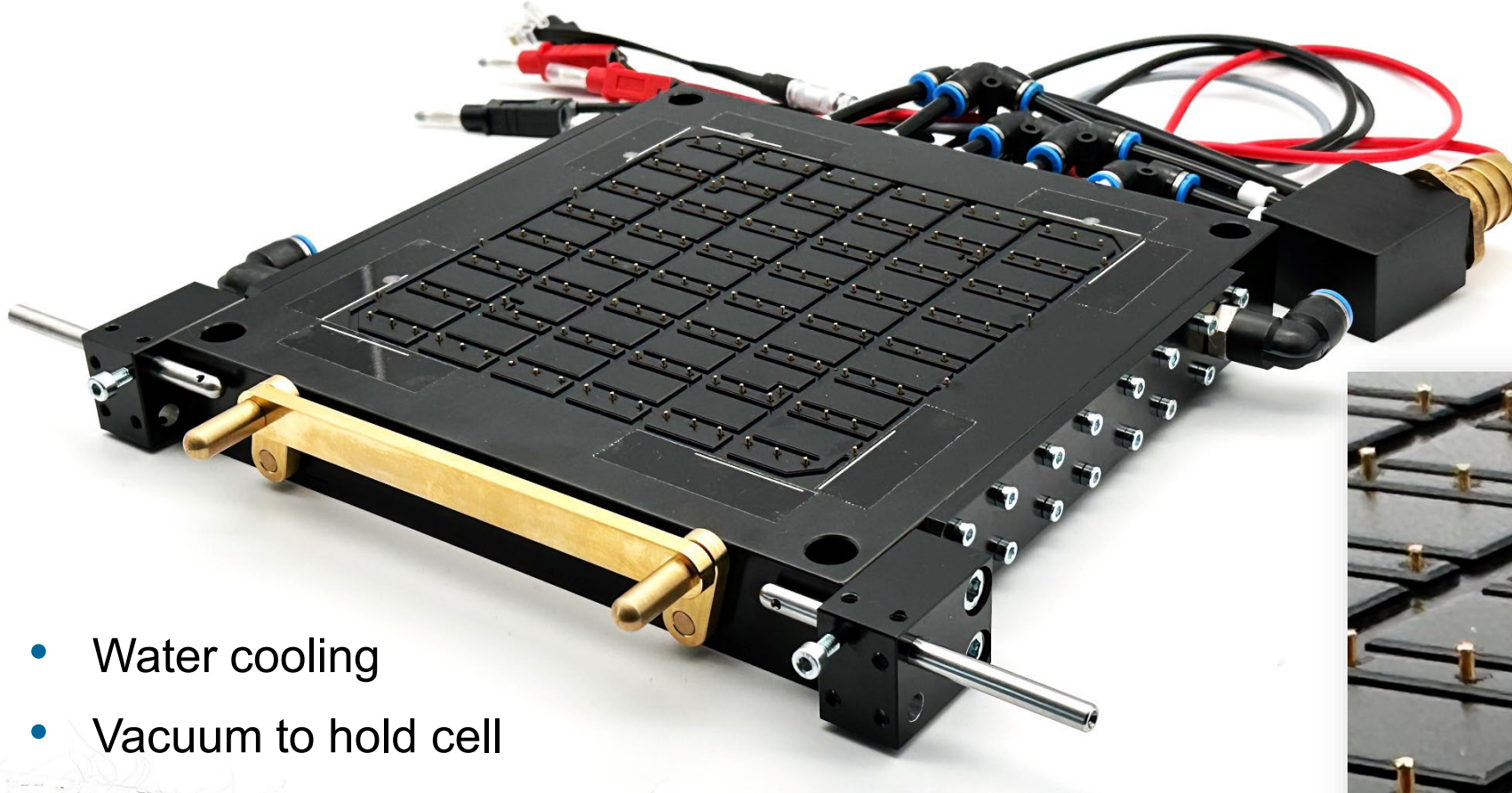
29.07.2024

Challenges in certified measurements of large-area Si solar cells

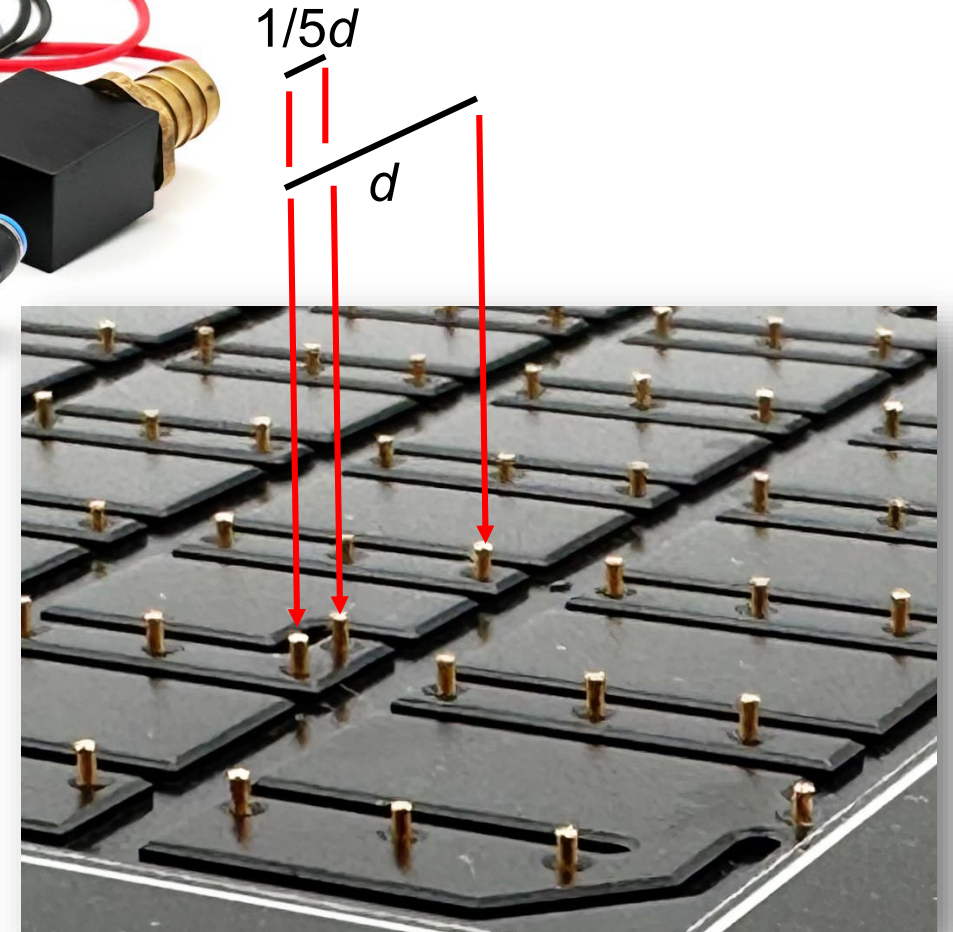
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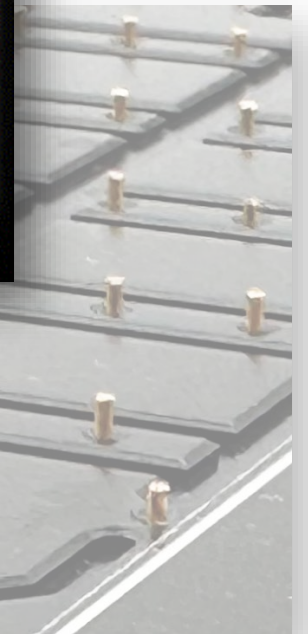
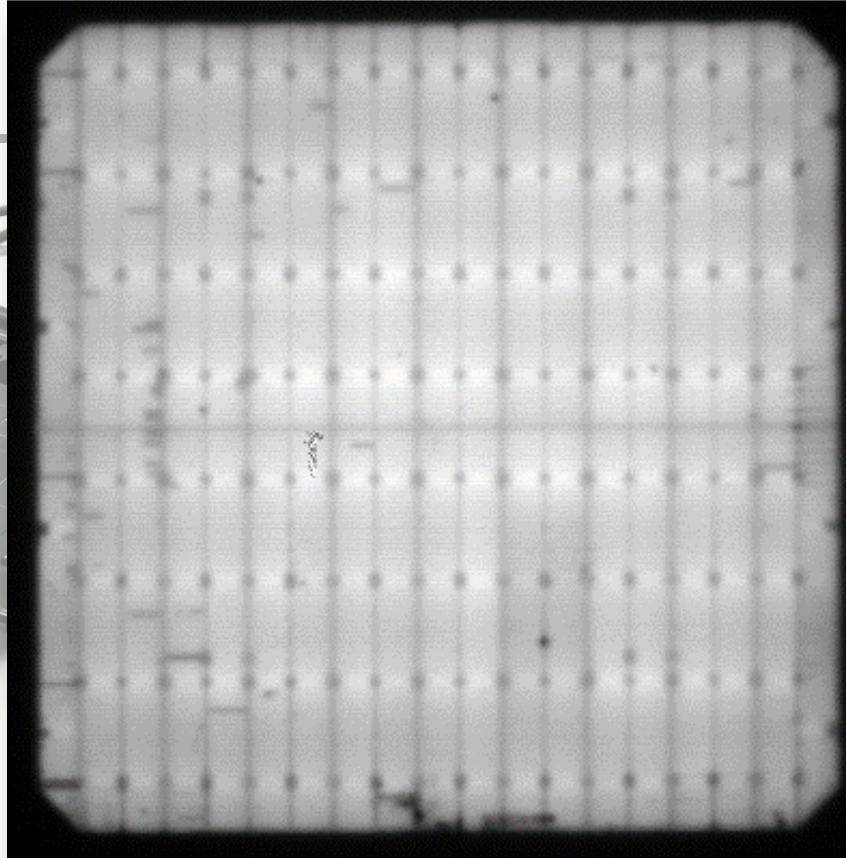
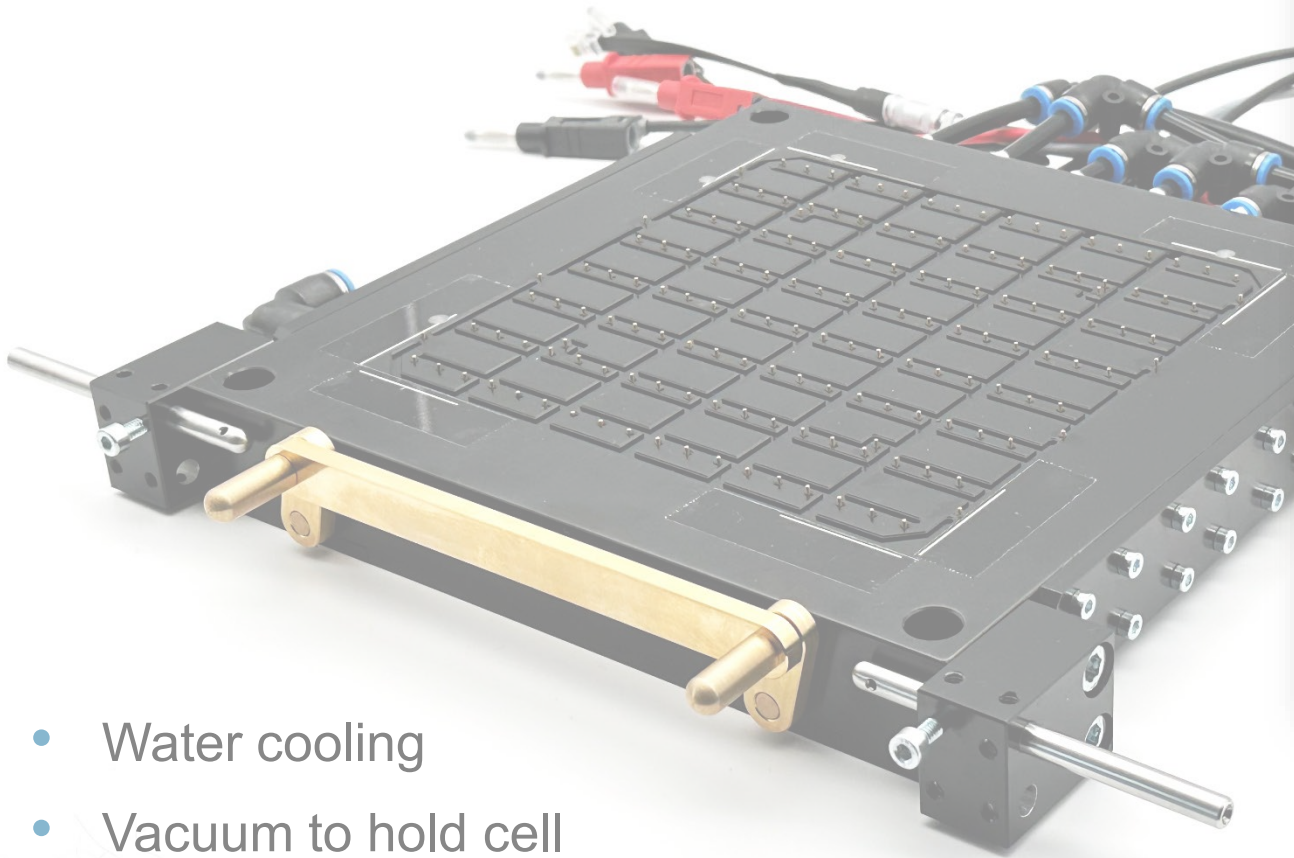
Contacting bare back contact cells – fakir chuck



- Water cooling
- Vacuum to hold cell
- Correct sensing
- Homogenous contacting

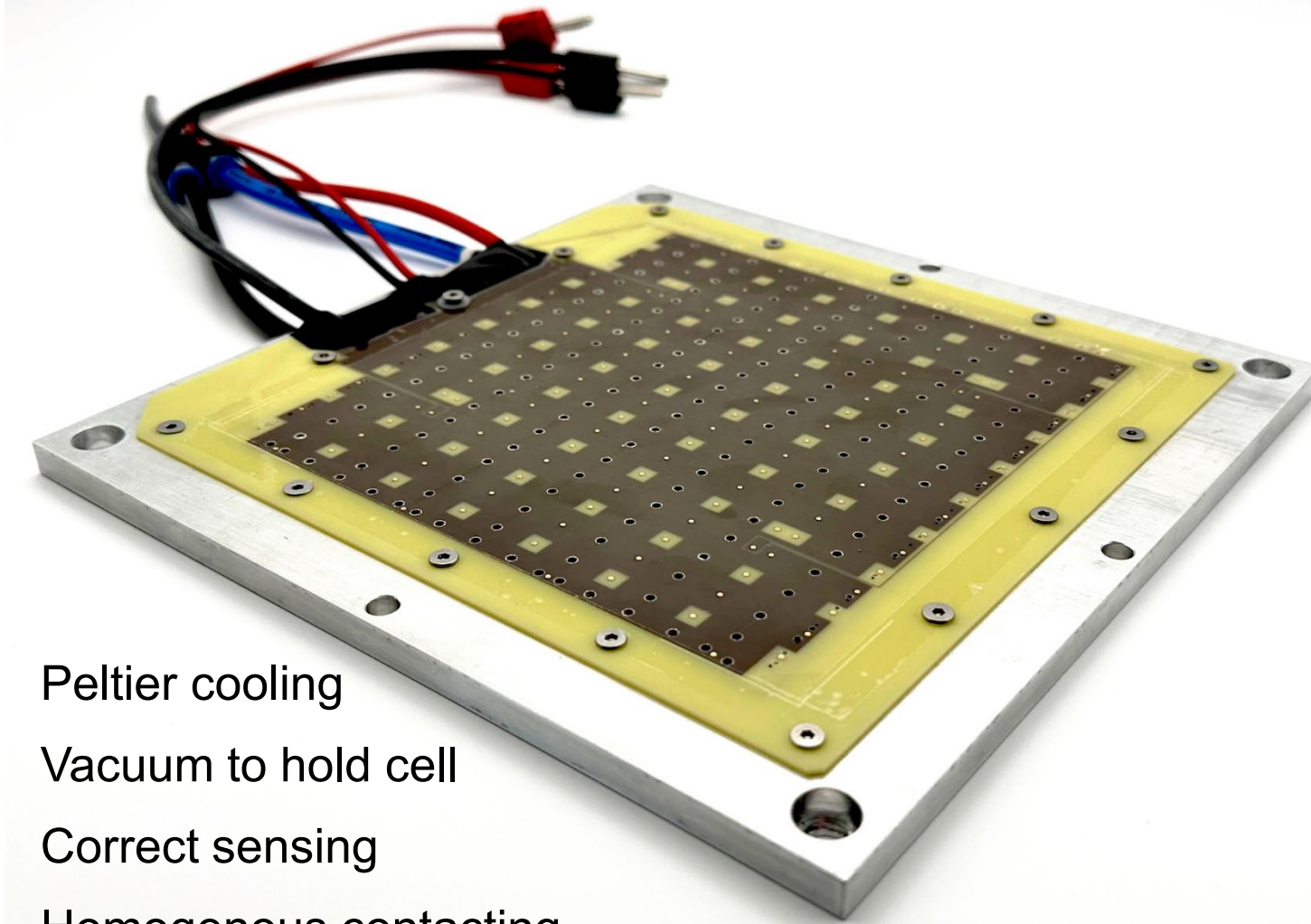


Contacting bare back contact cells

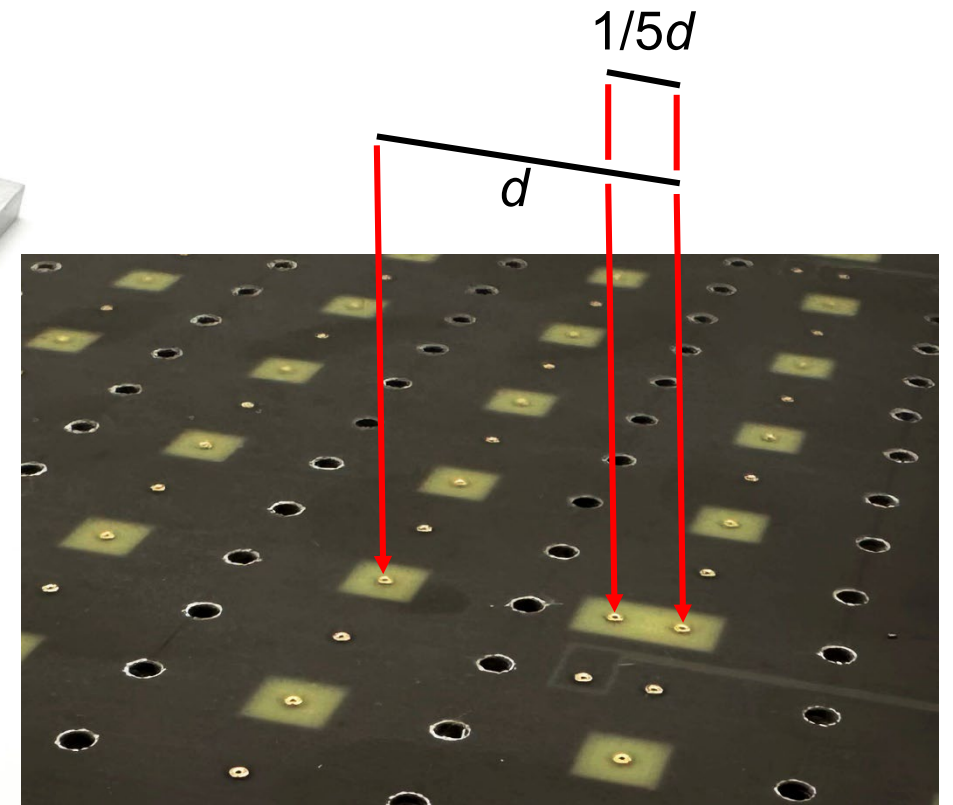


- Water cooling
- Vacuum to hold cell
- Correct sensing
- Homogenous contacting

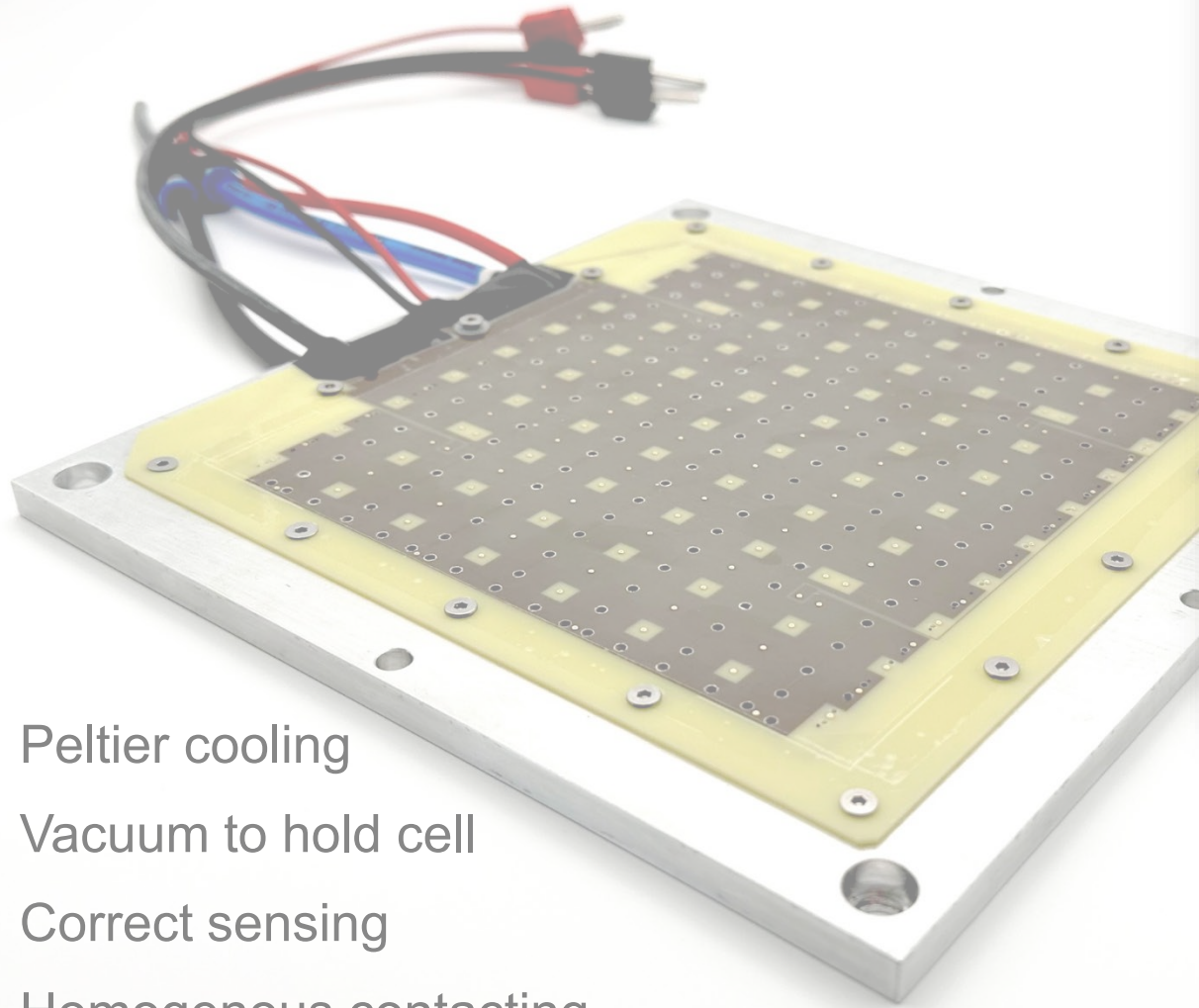
Contacting bare back contact cells – PCB chuck



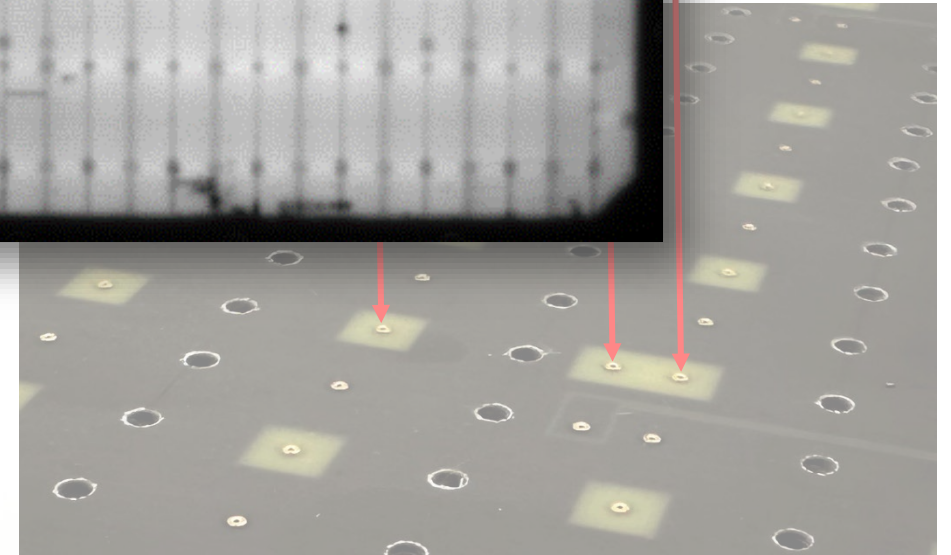
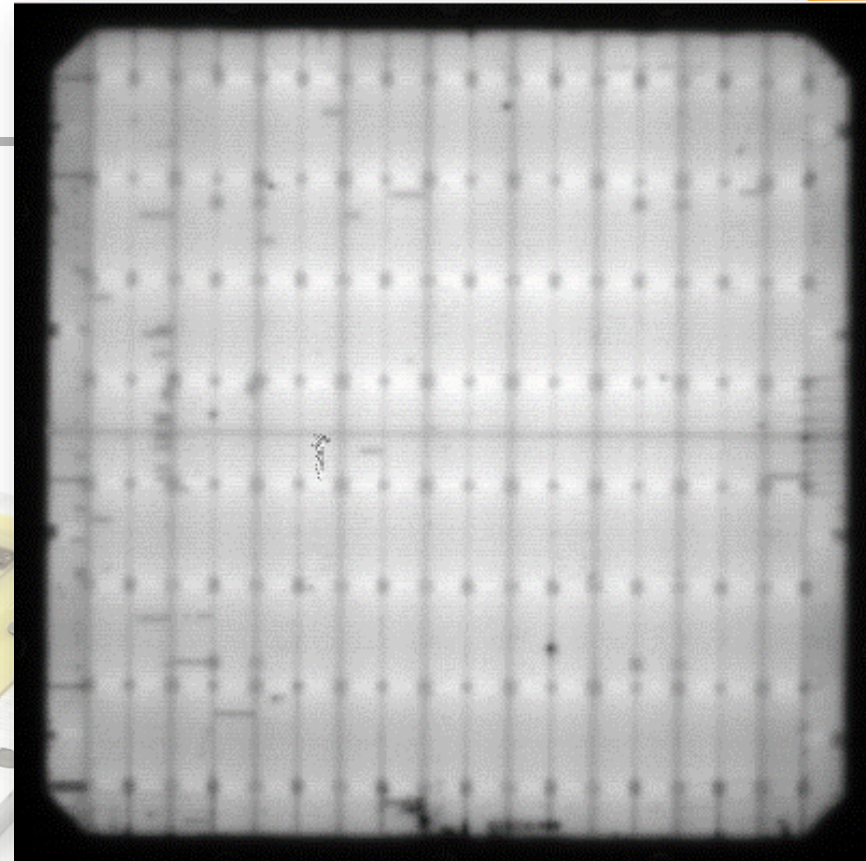
- Peltier cooling
- Vacuum to hold cell
- Correct sensing
- Homogenous contacting

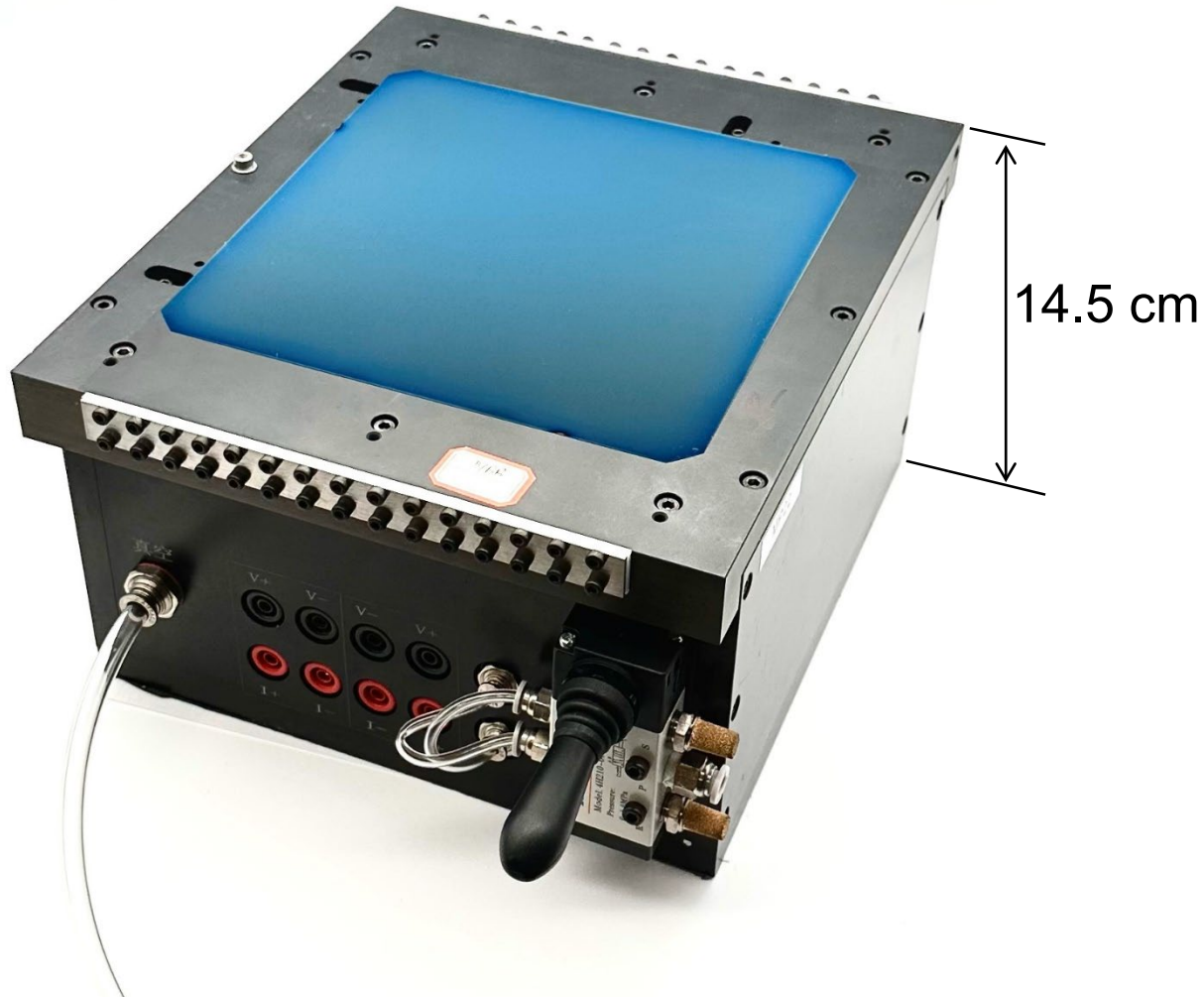


Contacting bare back contact cells



- Peltier cooling
- Vacuum to hold cell
- Correct sensing
- Homogenous contacting





Acceptance tests (selected criteria):

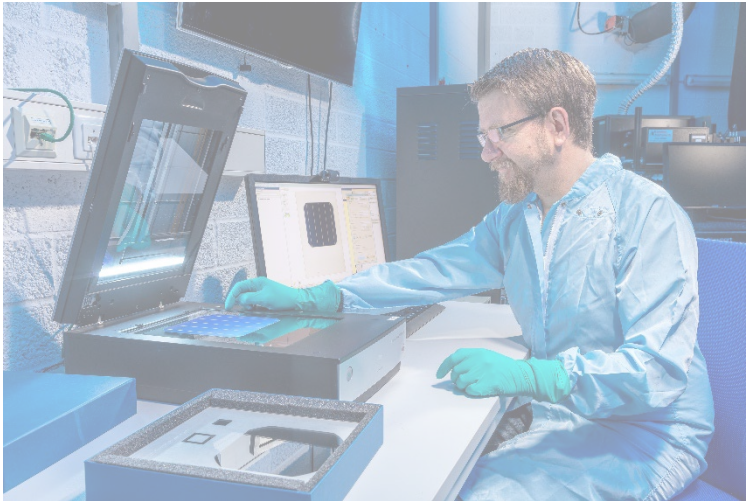
- Temperature:
 - Thermal contact area > 50%
 - Thermalization to 25°C under illumination possible
 - Temperature homogeneity better than ± 0.25 °C
- Electrical contact:
 - 4-wire contacting realized
 - Sense contact position correct
 - Robustness of cables, plugs and sockets OK
 - Lateral EL distribution only due to cell "features" (busbar & finger resistance, wafer inherent or process induced defects) not due to bad contacting pins (inhomogeneous contacting resistance)
 - Reproducibility of V_{OC} better than ± 0.3 mV
 - Reproducibility of $FF \pm 0.3$ %_{abs}

Calibration of solar cells in three steps

Area (cell (TA) or mask (DA))

Spectral Responsivity

Current-Voltage Characteristic



- Required for efficiency calculation



- Required for spectral mismatch correction
- Provides information about linearity

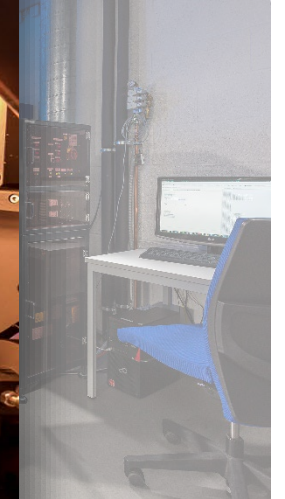


- Required for determination of characteristic parameters I_{sc} , V_{oc} , P_{max} , FF and efficiency

Calibration

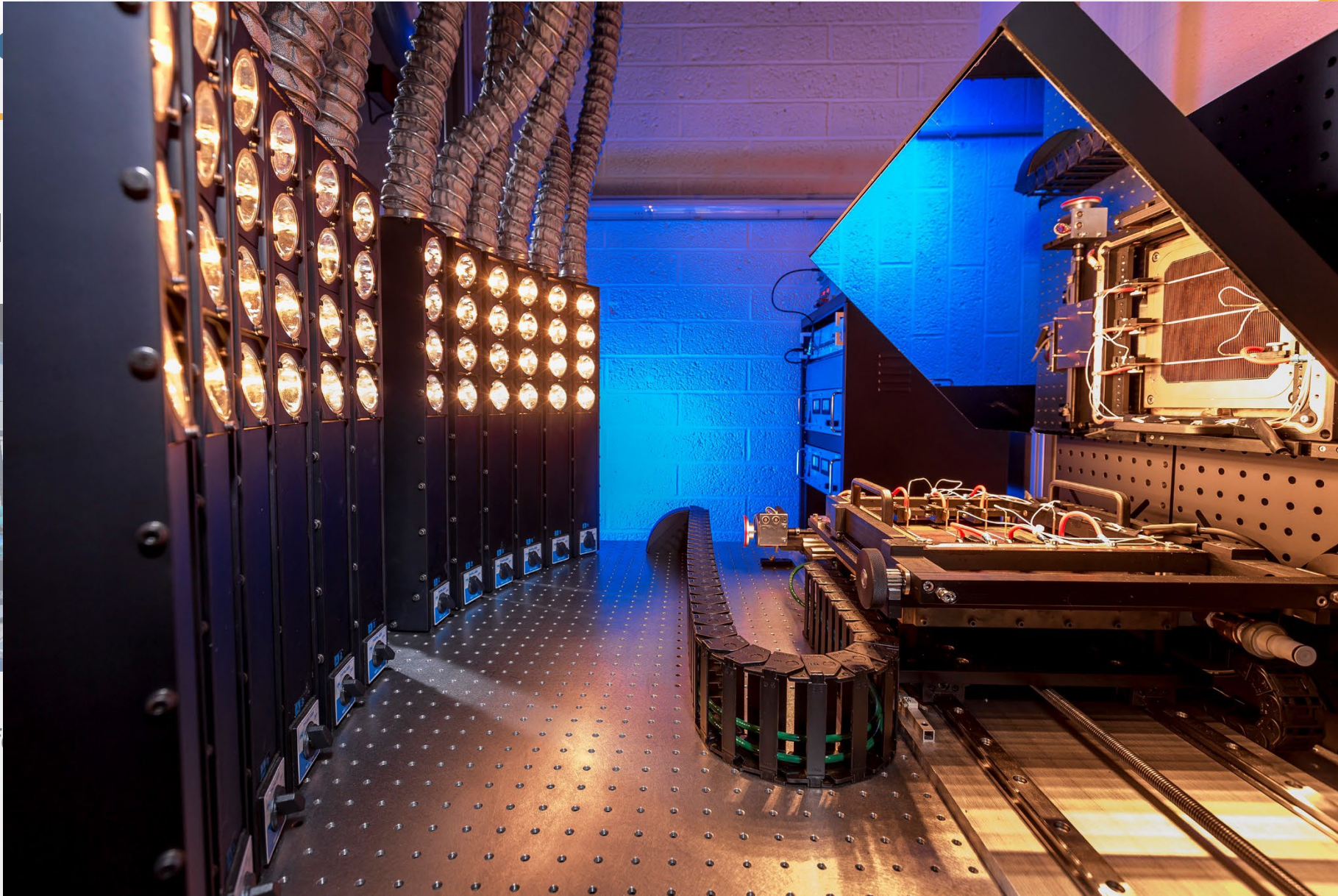
Area (cell

racteristic

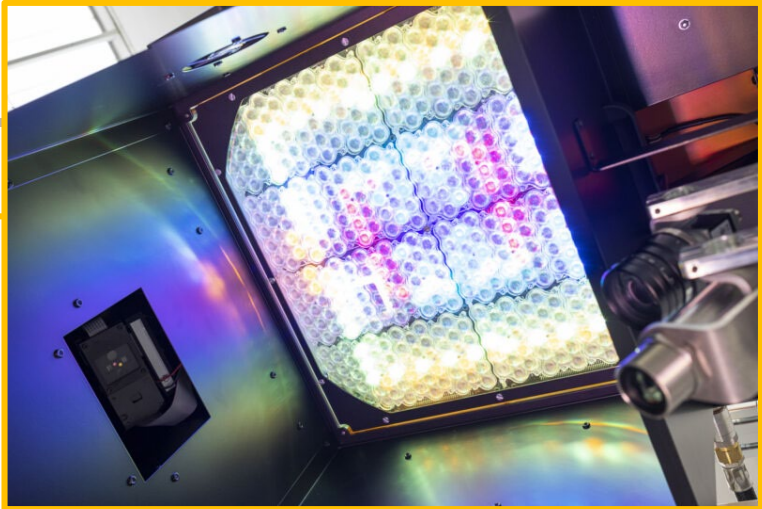


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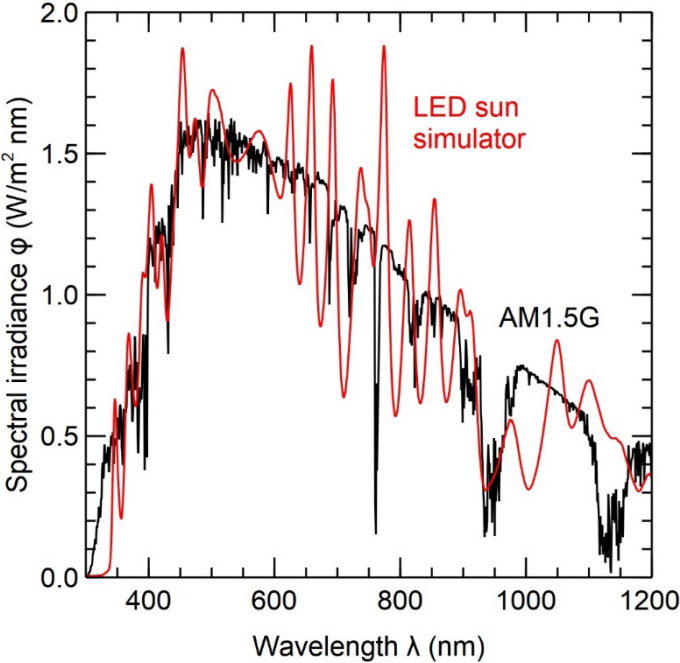
tion of
rs I_{sc} , V_{oc} ,



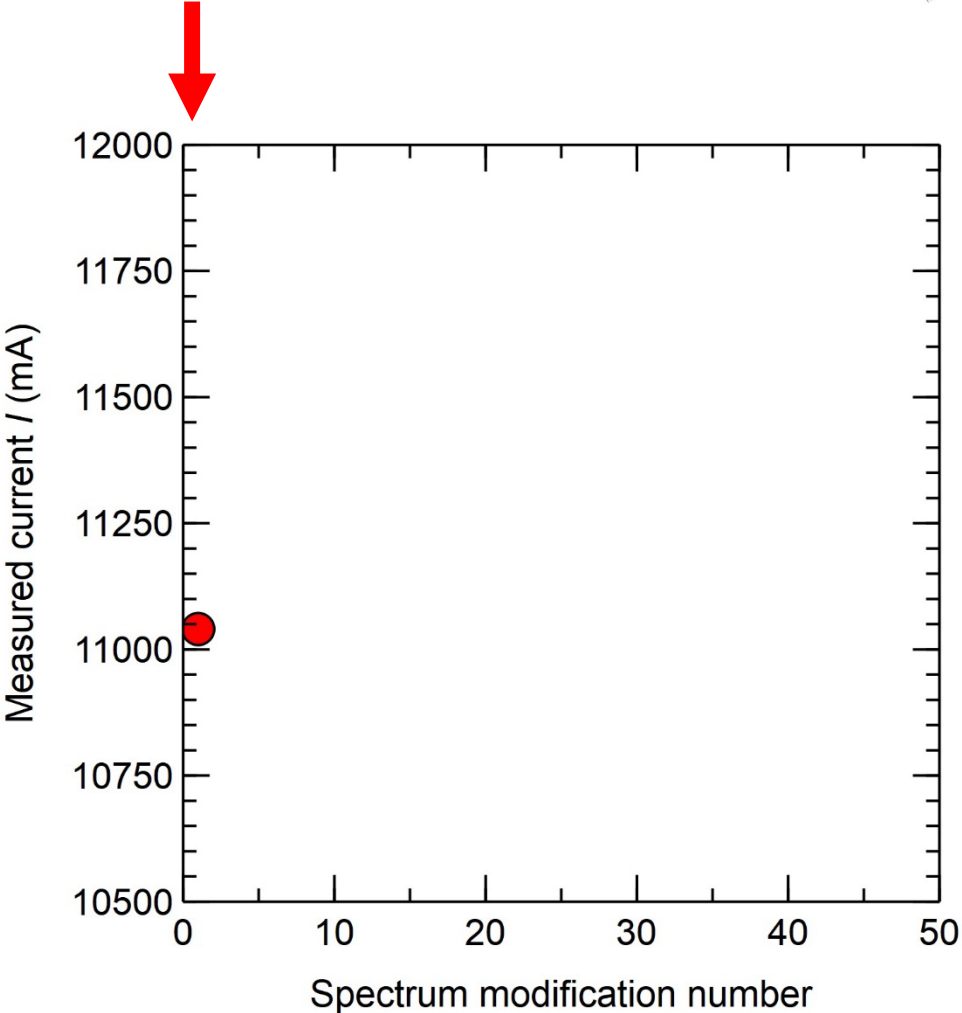
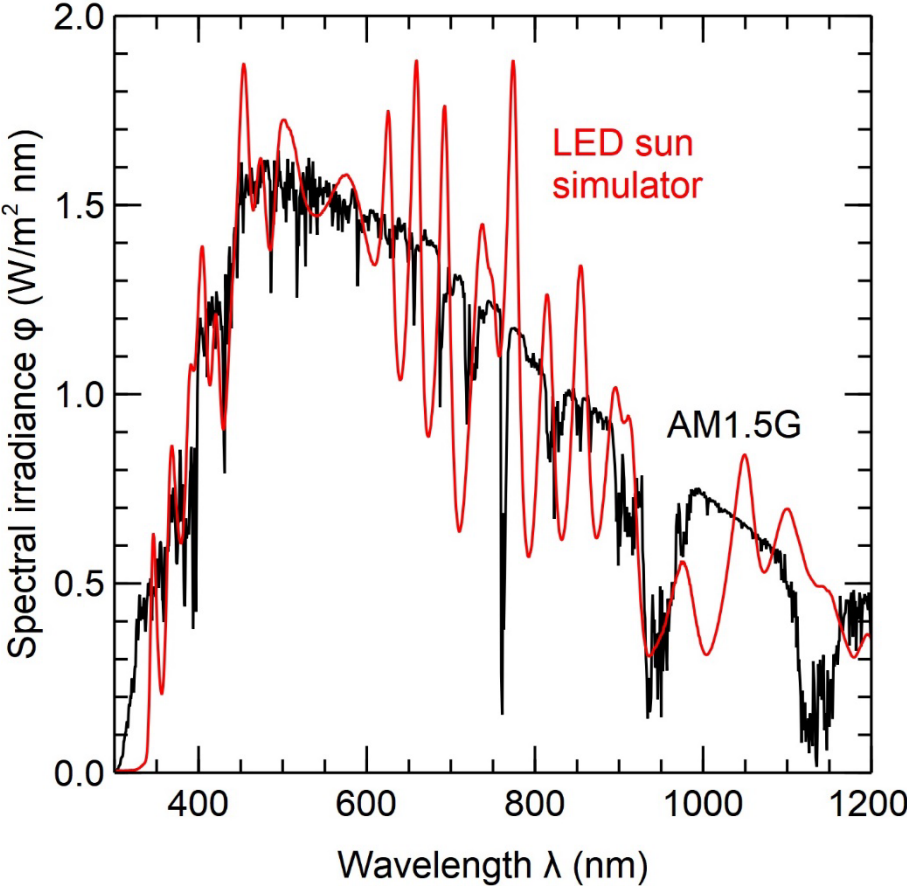
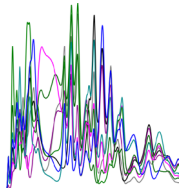
LED sun simulators



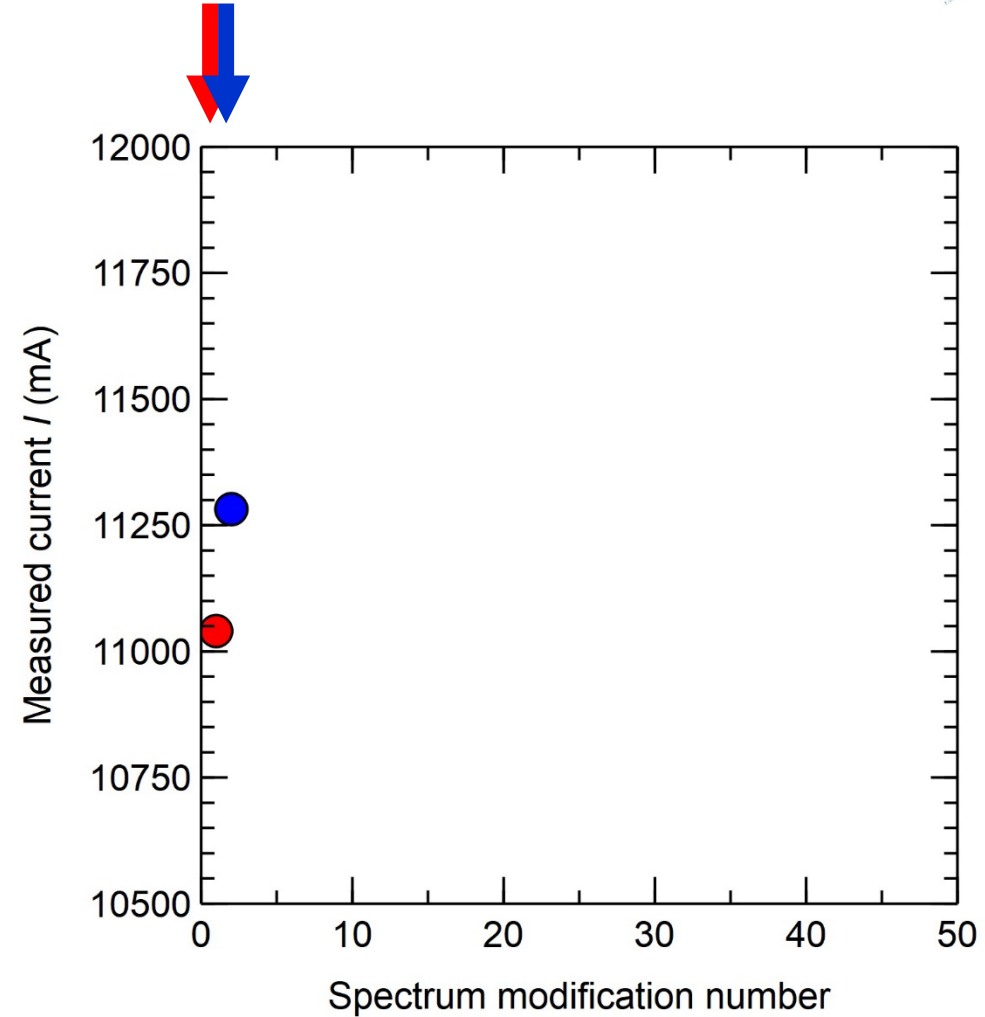
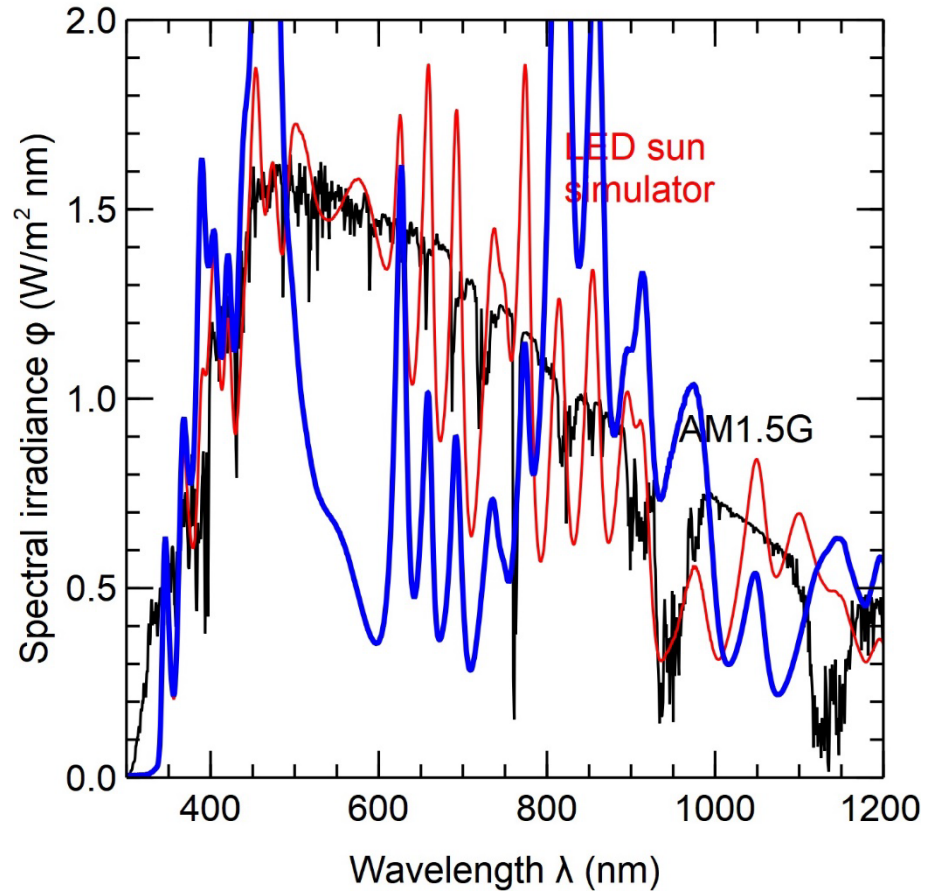
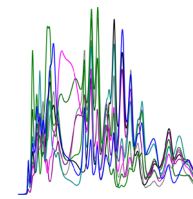
Picture from WAVELABS Solar Metrology Systems GmbH



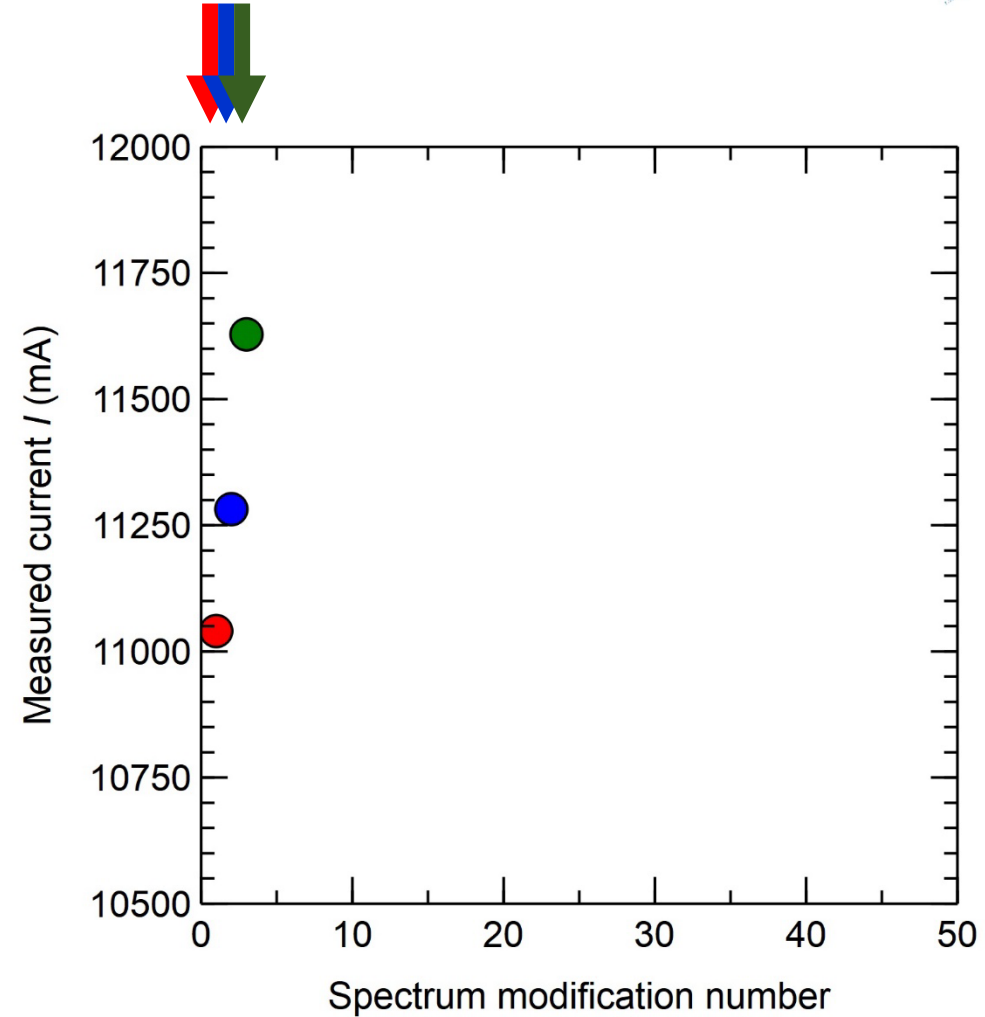
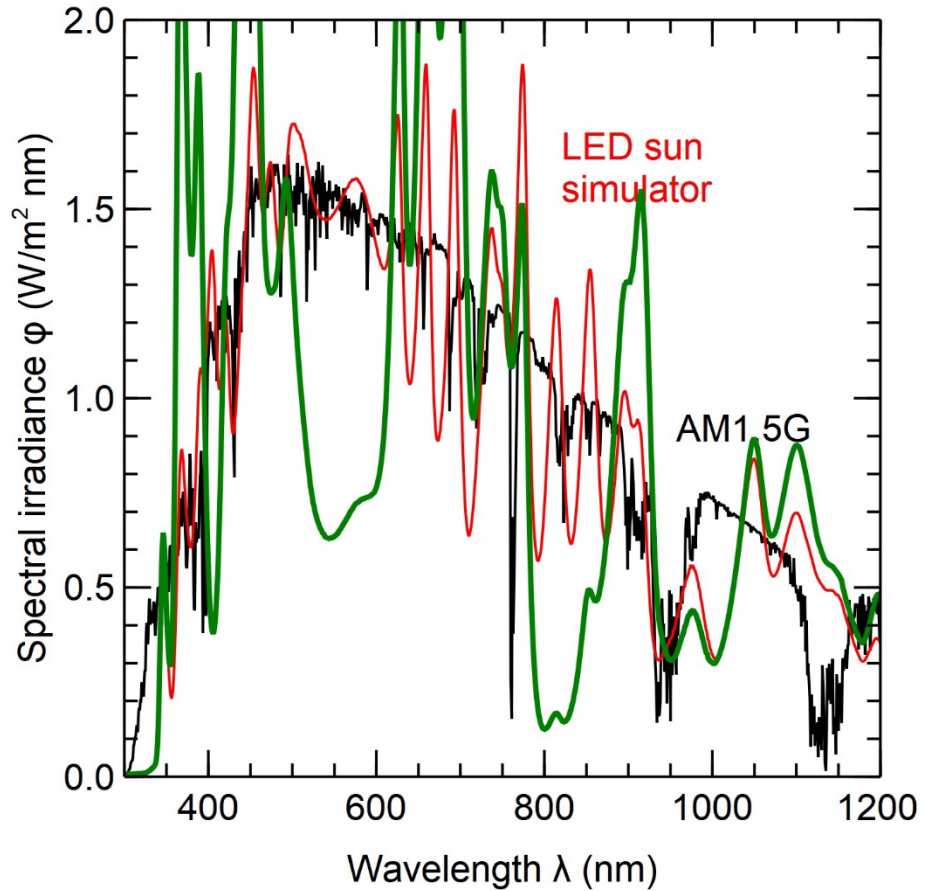
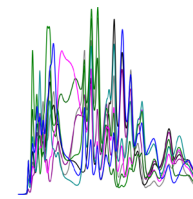
Base spectrum



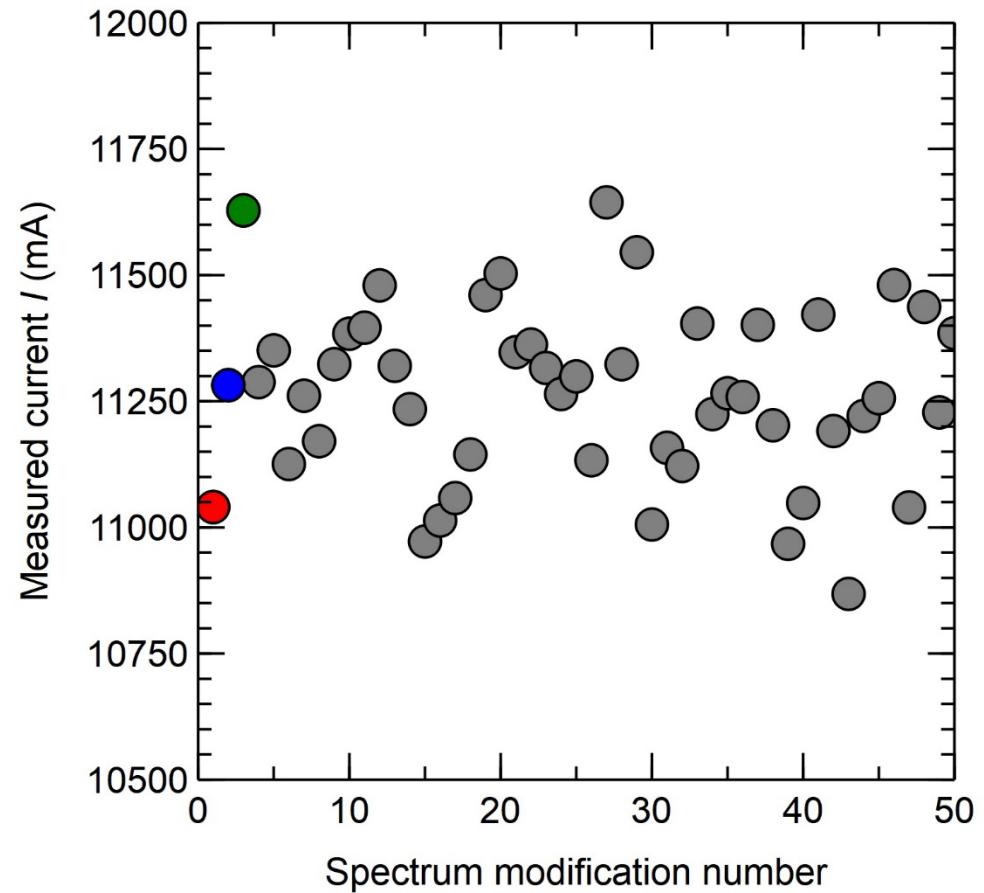
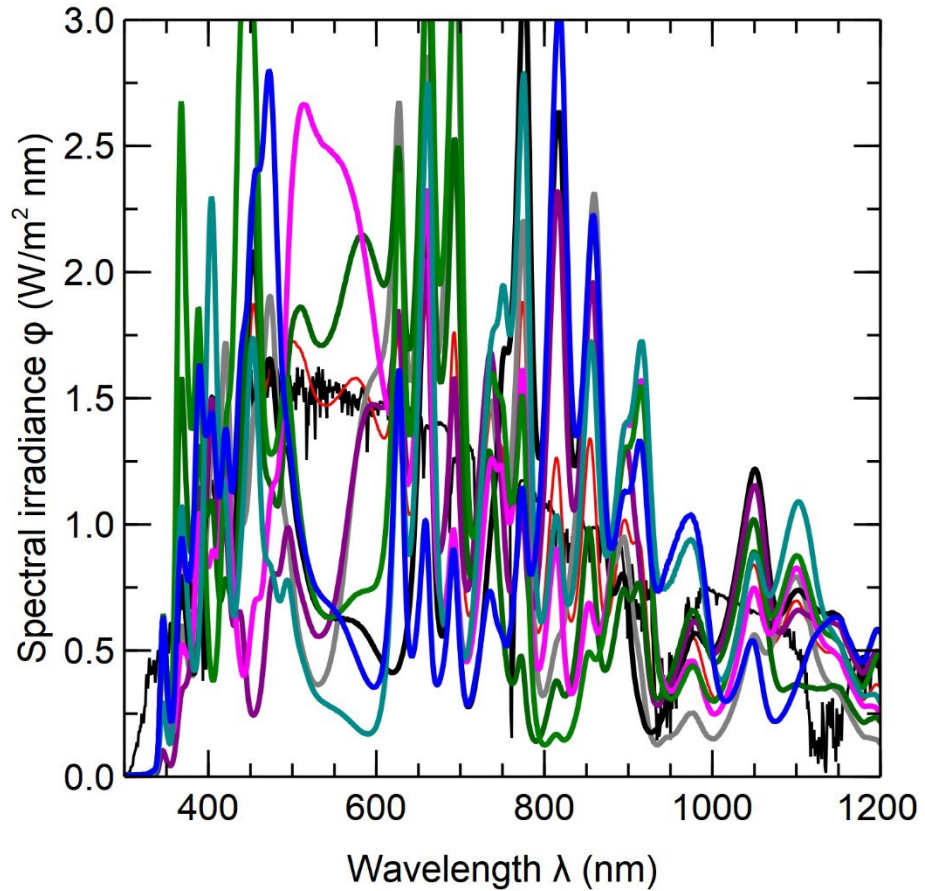
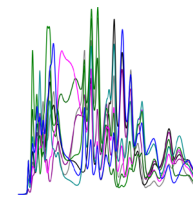
Spectral modification 1



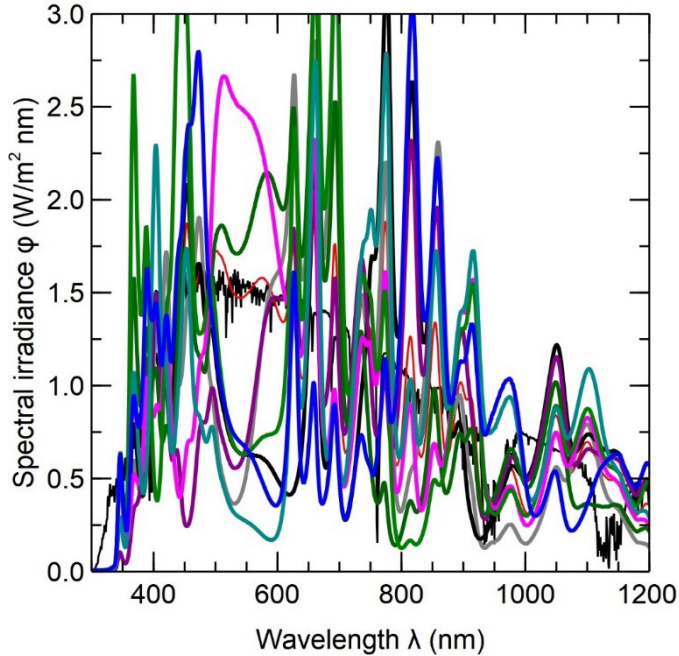
Spectral modification 2



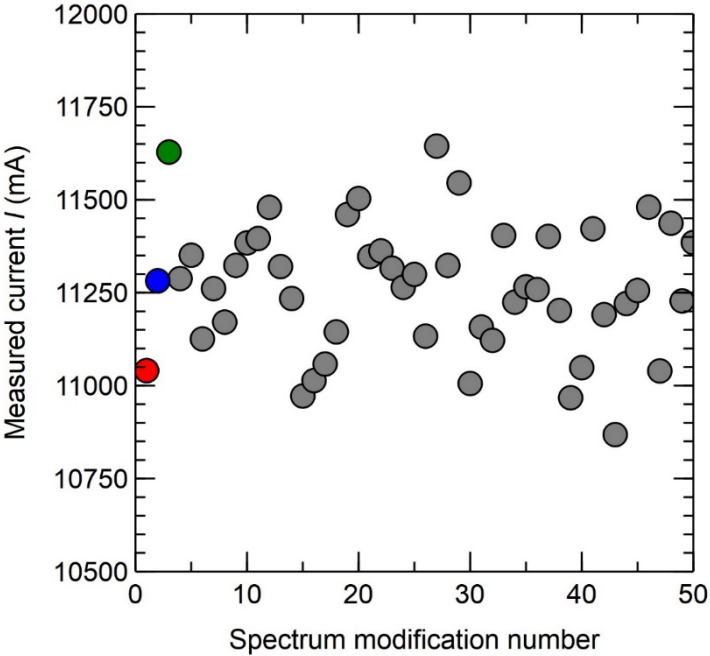
Spectral modification 1 to 50



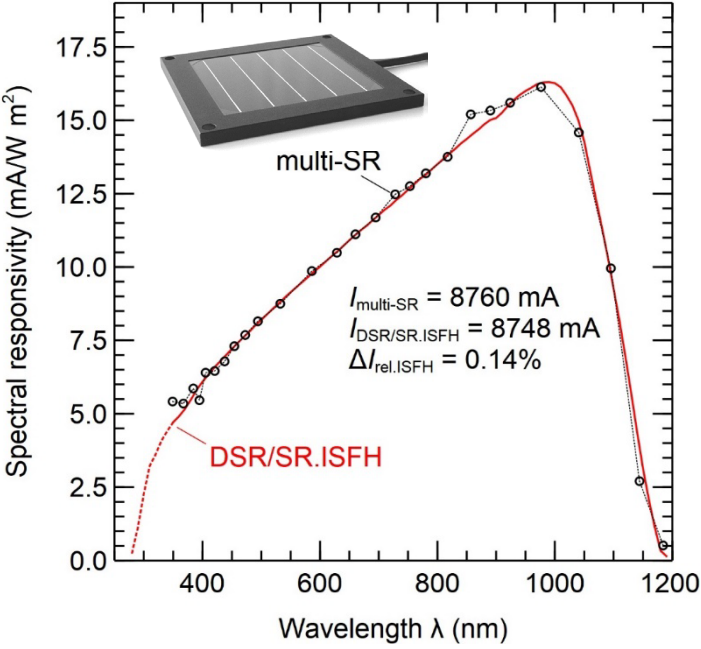
Multi-spectrum SR using a LED solar simulator



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Research Article

Multi-Spectrum Method for the Determination of the Spectral Responsivity and the Short-Circuit Current of Photovoltaic Devices

David Hinken, Carsten Schinke, Karsten Bothe, Rolf Brendel

First published: 12 May 2023 | <https://doi.org/10.1002/solr.202300240>

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Abstract


Herein, a method for the determination of the spectral responsivity (SR) and the short-circuit current under standard test conditions of photovoltaic devices (e.g., solar cells) is presented. This multi-spectrum SR method requires a spectrally tunable broadband light

(12) NACH DEM VERTRAG ÜBER DIE INTERNATIONALE ZUSAMMENARBEIT AUF DEM GEBIET DES PATENTWESENS (PCT) VERÖFFENTLICHTE INTERNATIONALE ANMELDUNG

(19) Weltorganisation für geistiges Eigentum
Internationales Büro

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(74) Anwalt: **QIP PATENTANWÄLTE, DR. KUEHN & PARTNER MBB**; Bavariaring 10, 80336 München (DE).

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(54) Title: APPARATUS AND METHOD FOR MULTISPECTRAL DETERMINATION OF SPECTRAL IRRADIANCE SENSITIVITY AND VOLTAGE-DEPENDENT CURRENT BEHAVIOR OF PHOTOVOLTAIC UNITS

Record BC cells calibrated at ISFH

Progress in Photovoltaics: Research and Applications

WILEY

PROGRESS IN
PHOTOVOLTAICS

SHORT COMMUNICATION

Solar Cell Efficiency Tables (Version 65)

Martin A. Green¹ | Ewan D. Dunlop² | Masahiro Yoshita³ | Nikos Kopidakis⁴ | Karsten Bothe⁵ | Gerald Siefer⁶ | Xiaojing Hao¹ | Jessica Yajie Jiang¹

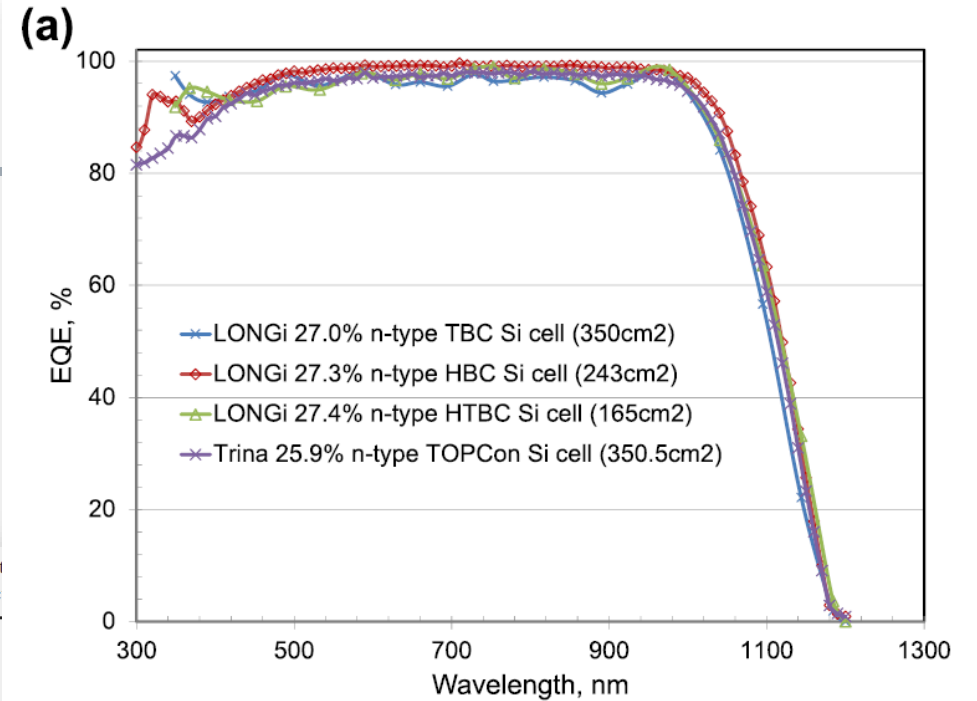


TABLE 2 | 'Not global AM1.5 spec'

Classification

Cells (silicon)

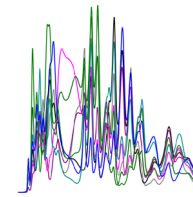
Si	25.0 ± 0.5	4.00 (da)	0.706	42.7 ^a	82.8	Sandia (3/99)	UNSW, p-type PERC [30]
	0.7241	42.87 ^c	83.1	FhG-ISE (7/17)	FhG-ISE, n-type TOPCon [31]		
	0.7323	42.05 ^d	84.3	FhG-ISE (11/19)	FhG-ISE, p-type TOPCon		
	0.7266	42.62 ^e	84.3	ISFH (2/18)	ISFH, p-type TBC [32]		
	0.6940	41.58 ^g	83.3	ISFH (7/19)	LONGi, p-type PERC [33]		
	0.7383	41.70ⁱ	84.1	ISFH (10/24)	TRINA, n-type TOPCon [34]		
Si (large)	27.0 ± 0.5^j	350.0 (t)	0.7447	42.32^k	85.8	ISFH (8/24)	LONGi, n-type TBC [4]
Si (large)	26.8 ± 0.4 ^l	274.4 (t)	0.7514	41.45 ^m	86.1	ISFH (10/22)	LONGi, n-type HJT [35]
Si (large)	26.6 ± 0.4 ^l	274.1 (t)	0.7513	41.30 ^m	85.6	ISFH (10/22)	LONGi, p-type HJT [36]
Si (large)	27.3 ± 0.4ⁿ	243.1 (da)	0.7434	42.60^k	86.2	ISFH (12/23)	LONGi, n-type HBC [4]

TABLE 1 | Confirmed single-junction terrestrial cell and submodule efficiencies measured under the global AM1.5 spectrum (1000 W/m²) at 25°C (IEC 60904-3: 2008 or ASTM G-173-03 global).

Classification	Efficiency (%)	Area (cm ²)	V _{oc} (V)	J _{sc} (mA/cm ²)	Fill factor (%)	Test centre (date)	Description
Silicon							
Si (crystalline cell)	27.4 ± 0.4^a	165.72 (t)	0.7456	42.35^b	86.7	ISFH (9/24)	LONGi, n-type HTBC [4]
Si (thin transfer submodule)	21.2 ± 0.4	239.7 (ap)	0.687 ^c	38.50 ^{c,d}	80.3	NREL (4/14)	Solexel (35 μm thick) [5]
Si (thin-film minimodule)	10.5 ± 0.3	94.0 (ap)	0.492 ^c	29.7 ^{c,e}	72.1	FhG-ISE (8/07)	CSG Solar (< 2 μm on glass) [6]

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Thank you for your attention!



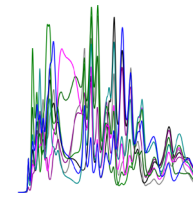
Equation system 1:

$$I_{sc1} = \int d\lambda \varphi_1(\lambda)SR(\lambda)$$

$$I_{sc2} = \int d\lambda \varphi_2(\lambda)SR(\lambda)$$

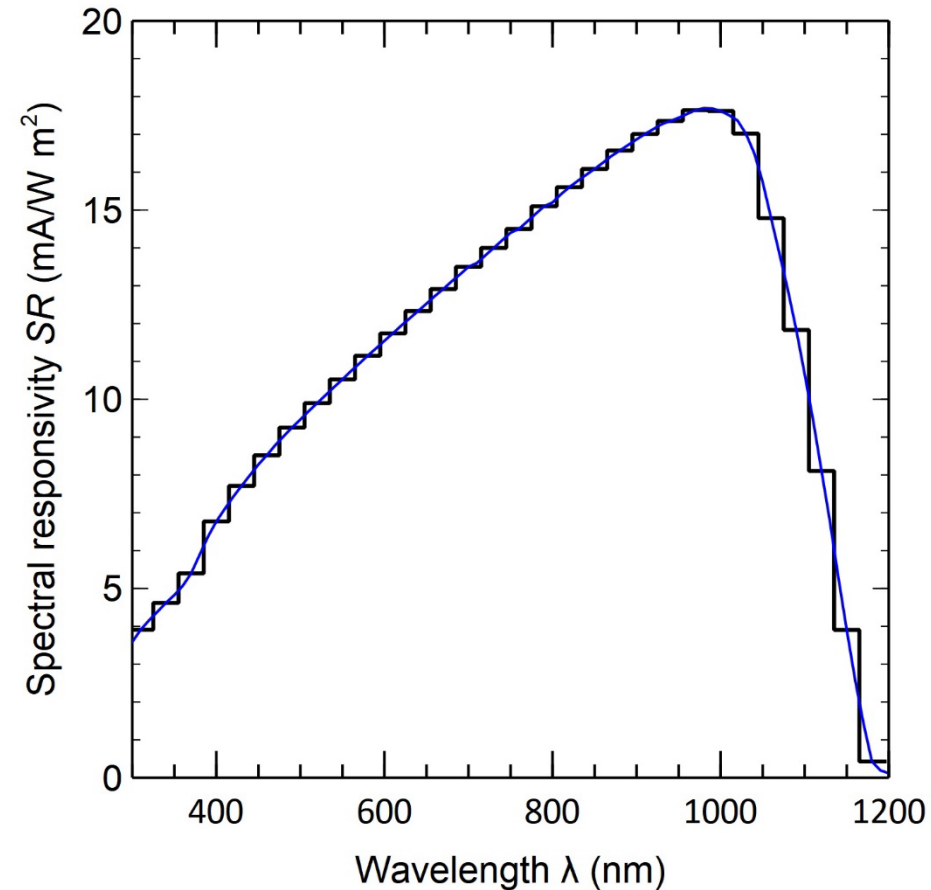
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$$I_{scM} = \int d\lambda \varphi_M(\lambda)SR(\lambda)$$

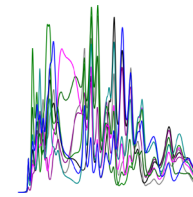


Equation system 1:

$$\begin{aligned} I_{sc1} &= \int d\lambda \varphi_1(\lambda) SR(\lambda) \\ I_{sc2} &= \int d\lambda \varphi_2(\lambda) SR(\lambda) \\ &\vdots \\ &\vdots \\ &\vdots \\ I_{scM} &= \int d\lambda \varphi_M(\lambda) SR(\lambda) \end{aligned}$$



- Discretization of SR curve into N intervals
- Obtain second equation system



Equation system 1:

$$\begin{aligned} I_{sc1} &= \int d\lambda \varphi_1(\lambda) SR(\lambda) \\ I_{sc2} &= \int d\lambda \varphi_2(\lambda) SR(\lambda) \\ &\vdots \\ &\vdots \\ &\vdots \\ I_{scM} &= \int d\lambda \varphi_M(\lambda) SR(\lambda) \end{aligned}$$

Equation system 2:

$$\begin{aligned} I_{sc1} &= \sum_{k=1}^N \int_{\lambda_k}^{\lambda_{k+1}} d\lambda \varphi_1(\lambda) SR_k \\ I_{sc2} &= \sum_{k=1}^N \int_{\lambda_k}^{\lambda_{k+1}} d\lambda \varphi_2(\lambda) SR_k \\ &\vdots \\ &\vdots \\ &\vdots \\ I_{scM} &= \sum_{k=1}^N \int_{\lambda_k}^{\lambda_{k+1}} d\lambda \varphi_M(\lambda) SR_k \end{aligned}$$

- Discretization of SR curve into N intervals
- Obtain second equation system
- Solvable with least-square algorithm with N unknowns
- Result: SR_1, \dots, SR_N